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Spherical harmonic analysis of earth's conductive heat flow

V. M. Hamza · R. R. Cardoso · C. F. Ponte Neto

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Abstract A reappraisal of the international heat flow database has been carried out and the corrected data set was employed in spherical harmonic analysis of the conductive component of global heat flow. Procedures used prior to harmonic analysis include analysis of the heat flow data and determination of representative mean values for a set of discretized area elements of the surface of the earth. Estimated heat flow values were assigned to area elements for which experimental data are not available. However, no corrections were made to account for the hypothetical effects of regional-scale convection heat transfer in areas of oceanic crust. New sets of coefficients for 12° spherical harmonic expansion were calculated on the basis of the revised and homogenized data set. Maps derived on the basis of these coefficients reveal several new features in the global heat flow distribution. The magnitudes of heat flow anomalies of the ocean ridge segments are found to have mean values of less than 150 mW/m^2 . Also, the mean global heat flow values for the raw and binned data are found to fall in the range of 56–67 mW/m^2 , down by nearly 25% compared to the previous estimate of 1993, but similar to earlier assessments based on raw data alone. To improve the spatial resolution of the heat flow anomalies, the spherical harmonic expansions have been extended to higher degrees. Maps derived using coefficients for 36° harmonic expansion have allowed identification of new features in regional heat flow fields of several oceanic and continental segments. For example, lateral extensions of heat flow anomalies of active spreading centers have been outlined with better resolution than was possible in earlier studies. Also, the characteristics of heat flow variations in oceanic crust away from ridge systems are found to be typical of conductive cooling of the lithosphere, there being little need to invoke the hypothesis of unconfined hydrothermal circulation on regional scales. Calculations of global conductive heat loss, compatible with the observational data set, are found to fall in the range of 29–34 TW, nearly 25% less than the 1993 estimate, which rely on one-dimensional conductive cooling models.

Keywords Global heat flow .

Spherical harmonic analysis · Conduction heat transfer

Introduction

Since the pioneering work by Everett (1883), several attempts have been made to estimate mean heat flow of the earth, based on results of experimental heat flow measurements. These include, among others, the works of Birch (1954), Lee and Uyeda (1965), Horai and Simmons (1969), Chapman and Pollack (1975) and Jessop et al. (1976). Since the decade of 1970 significant progress has been achieved in data acquisition, with direct determination of heat flow in several major tectonic regions of the earth. However, the improvements in the global data base have not lead to substantial changes in these earlier estimates. Nevertheless, in presenting the updated compilation of global heat flow data, Pollack et al. (1993) arrived at an estimate of 87 mW/m² for the mean heat flow of the earth, which is nearly 30% higher than the previous ones. An examination of their procedure reveals that the estimate of high mean heat flow is not based on experimental data, but a consequence of the large-scale use of theoretical values for large segments of the young oceanic crust. Pollack et

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al. (1993) justify this procedure on the ground that experimental heat flow values for the ocean crust do not account for heat transfer by hydrothermal activity and hence are not representative of the total heat flux. The implicit assumption behind this argument is that active unconfined hydrothermal systems operate on regional scales in large parts of the oceanic crust, and that a one-dimensional conductive cooling model correctly account for the difference.

In our understanding the hypothesis of unconfined hydrothermal circulation (which is the basis for the use of theoretical heat flow values) is questionable in the light of available information on the thermal and hydrological characteristics of the ocean crust. The relevant information may be summarized as follows:

- 1. The presence of hydrothermal convection in deeper lavers of the oceanic crust need not necessarily lead to systematic errors in conductive heat flow values. In much of the ocean crust the upper layer of basaltic rocks, where fluid circulation is believed to take place, is overlain by low permeability sediments. Under such conditions, the sedimentary layer act as a confining lid on underlying hydrothermal circulation systems. Measurements of conductive heat transfer in such confining layers are known to provide reasonable estimate of background heat flux (Garg and Kassoy 1981; Holst and Aziz 1972; Ribando and Torrance 1976). Only in areas of unconfined circulation does conduction heat transfer lead to underestimation of total heat loss (Cheng and Lau 1974; Pratts 1966);
- 2. Direct evidences pointing to the occurrence of heat transfer by thermal fluid discharges in the ocean floor are limited to faults and fracture zones situated in ridge crests and ridge flanks of active spreading centers (Baker et al. 1996; Embley et al. 1991; German et al. 1994; Haymon et al. 1991; Lupton et al. 1993; Murton et al. 1994; Williams et al. 1974 among others). Fluid discharges emanating from deep circulation systems are rare in areas of ocean crust away from spreading centers. It is not a ubiquitous heat transfer process operating in ocean crust blanketed by sediments;
- 3. Marine heat flow measurements are usually neither preceded nor accompanied by detailed mapping of local fracture zones and fluid circulation systems of the ocean floor (Lubimova et al. 1965; Jones 1999). Given the lack of knowledge of the mechanical, thermal and hydrological characteristics of underlying rock strata, it seems reasonable to assume that the sites of heat flow measurements are randomly distributed with respect to the fracture systems. In such cases, heat flow values averaged over large area elements are unlikely to lead to biased estimates;

- 4. The sedimentary layers in the ocean floor are characterized by relatively low permeability (10⁻¹⁸-10⁻¹⁴ m²/s), which is several orders of magnitude less than the permeability of fracture zones in basalts (Becker and Davis 2003; Becker and Fisher 2000; Bryant et al. 1981; Fisher 1998; Giambalvo et al. 2000; Hamilton 1976 among others). The rapidly accumulating sediment cover over the young ocean crust is known to act as an impermeable barrier against widespread occurrence of unconfined hydrothermal systems (Snelgrove and Forster 1996);
- 5. In fault or fracture controlled hydrothermal systems the perturbations of heat flow field are generally limited to rather narrow belts of recharge and discharge zones (Goyal and Kassoy 1977; Gray et al. 1976 among others). The lateral dimensions of unperturbed areas lying between these zones are several orders of magnitude larger than those of fracture zones themselves (Alexandrino and Hamza 2005; Turcotte and Schubert 1982). Hence the probability that measurement sites are preferentially situated on or close to recharge zones of hydrothermal systems is relatively small. Randomly distributed measurements are unlikely to provide biased estimates of background heat flow;
- 6. Because of complexities in deep-sea operations and limitations of experimental techniques most of the oceanic heat flow measurements are carried out at sites where sedimentary cover is present (Jones 1999). In such areas the heat flow field is most likely unperturbed;
- 7. Chemical reactions and mineral precipitations lead to drastic reductions in permeability of the circulation systems over time-scales relatively short compared with the age of the oceanic lithosphere (Akaku 1988; Drummond and Ohmoto 1985; Lowell et al. 1993; Meyer and Hemley 1967). Under such conditions it is reasonable to assume that the permeability of fracture systems falls off rapidly with distance from the ridge areas. This appears to be a major limiting factor that inhibit occurrence of large-scale convective movements in the old ocean crust; and
- 8. The convection systems proposed for the ocean crust away from ridge zones have upwelling limbs situated in the relatively colder parts of the lithosphere and down-going limbs situated within the warmer parts. Such a situation is contrary to what is normally observed in natural thermal convection systems (Cheng 1978; Combarnous and Bories 1975; Elder 1981).

Other relevant factors to be considered in this context are the geochemical constraints on overall heat loss of the earth. As noted by Hofmeister and Criss (2005) these constraints lead to estimates that differ significantly from that of Pollack et al. (1993). Also, the comments by Von Herzen et al. (2005) on the recent work of Hofmeister and Criss (2005) and that by Hofmeister and Criss (2006) on the work of Wei and Sandwell (2006) indicate that there are considerable disagreements in the current assessments of global heat flow. Also, the parameters used by Pollack et al. (1993) are not appropriate, as shown by recent measurements of thermal conductivities. In this context, reexaminations of the primary geothermal data base and the procedures used in harmonic representations of global heat flow are in order.

The present work reports results of harmonic analysis of the revised global heat flow database, following a procedure that makes full use of the entire observational data set. Initially, a reassessment of the global heat flow database is carried out, based on the recent works of Ponte Neto and Hamza (2004), Cardoso et al. (2005) and Cardoso and Hamza (2006). The corrected data base is subsequently used in determining representative mean heat flow values for a regular grid system composed of $5^{\circ} \times 5^{\circ}$ area elements of the surface of the earth. Because the emphasis of the present work is in investigating conductive heat flow variations, we refrained from the practice of using theoretical heat flow values as a substitute for experimental data. The regularized data set is used to calculate new sets of harmonic coefficients and in deriving new global heat flow maps.

Reappraisal of the IHFC database

The global heat flow database in its present form is an outgrowth of earlier compilations by Birch (1954), Lee (1963), Lee and Uyeda (1965), Jessop et al. (1976) and Pollack et al. (1993). Progress in data acquisition during the decades prior to 1980 has not only lead to substantial improvements in outlining regional heat flow anomalies but also better representations of the global thermal field. Since 1990 however, advances in data acquisition has been relatively slow, being restricted mainly to areas of low data density in the Asian and South American continents.

The database available for download at the web site of NGDC includes 21,453 records of heat flow measurements over the globe. Of these 12,105 are on land, 9,053 in oceanic regions, and the remaining 295 in transition regions, such as continental platform areas and shallow water bodies. The format adopted for the individual fields of information has been discussed in detail by Balling et al. (1981), but the data set as a whole remains essentially as an intercalating system of tables and references. Only recently has steps been taken to implement spreadsheet based

systems, suitable for automatic processing (Gosnold, personal communication).

The database may be considered as composed of essentially three parts: continental, oceanic, and transition regions. These are further subdivided into several subsets. Regarding continental areas, the data for the different countries are grouped into separate tables. For oceanic regions several sets of data have been put together, following roughly the chronological order of heat flow measurements. Consequently, careful and detailed preprocessing is necessary for extracting data sets for the different tectonic units. Also, classification of data sets for continental platform areas, inland seas and water bodies do not appear to follow any consistent or systematic schemes. Such difficulties are probably the main underlying reason for the very few attempts, which have so far been made, in examining heat flow variations on a global scale.

The distribution of heat flow data over the globe is illustrated in Fig. 1. Recent compilations reported by Hamza and Muñoz (1996) and Hamza et al. (2005) were also included to improve the regional distribution for the South American continent. It is clear to note that the availability of data is reasonable in several of the major regional sectors and geotectonic units in both continental and oceanic regions. However, areas of poor data density exist in continental areas of North Africa, Central Asia, and South America, as well as in Polar regions of the northern and southern hemispheres. High latitude areas of southern oceans also have poor data coverage.

In carrying out a reappraisal of the IHFC database, it was considered important to check the internal consistency of the database. This, however, turned out to be a task that could not easily be automated, in view of the archaic structure of the database. To circumvent this problem a spread sheet based system was implemented, which allowed verification of the individual data fields. Detailed verification revealed widespread occurrence of transcription and/or typographic errors in the database, unnoticed in earlier studies. The verification also revealed that the



Fig. 1 Global distribution of heat flow data. The *black dots* indicate locations of measurements in oceanic areas whereas *red dots* indicate that in continental areas

classification systems adopted for data from continental platform areas, inland seas and water bodies do not follow a consistent pattern. Also, there are cases where heat flow data obtained as part of projects that span over more than one country are simply listed as belonging to the country of the principal investigator. Such problems have lead to some degree of confusion in analysis and interpretation of the data. As an illustrative example, consider the data set for Switzerland, which lists heat flow measurements for 104 localities. Only 78 of these are located within the country limits of Switzerland, the remaining ones are found to be in neighboring areas of France, Italy and Germany. Similar problems exist with data sets for many other countries in the continents of Asia, Africa, and North America.

Clearly, there is a need for restructuring and reformatting the database. Recently, Cardoso et al. (2005) and Cardoso (2006) have proposed corrections for the occurrence of what they call as "large-scale" errors in the coordinates. Table 1 provides a summary list of such corrections in the coordinates. Most of the corrections are for continental areas of Asia, Europe, and North America. A number of incorrect locations were also found for data from oceanic regions. No corrections were found necessary for the more recent data from South America and the Antarctic.

Previous representations of global heat flow

Early attempts for harmonic analyses of heat flow data were carried out by Lee and MacDonald (1963), Lee and Uyeda (1965) and Horai and Simmons (1969). The procedures employed in these early works rely on analytical methods that generate an over-determined set of equations based on experimental data, which in turn is solved for the unknown coefficients. This approach has the inherent weakness that the harmonic representations in areas devoid

Table 1 Summary list of corrections for the IHFC database

Region	Number of data		Total	
	Correct locations	Incorrect locations		
Africa	526	21	547	
Central America	83	1	84	
South America	822	0	822	
Antarctic	9	0	9	
Asia	3,967	365	4,332	
Europe	1,943	112	2,055	
North America	4,466	156	4,622	
Australia and Pacific	264	23	287	
Seas and Oceans	9,179	169	9,348	
Total	2,1259	847	2,2106	

of data are sensitive to numerical instabilities. In such cases, the values of the harmonic coefficients depend to a large extent on the data density and also characteristics of the data distribution.

In the work of Chapman and Pollack (1975), hereafter abbreviated as C&P, problems arising from uneven data distribution are minimized by employing discretized data sets and using estimated values for grid elements for which experimental data are not available. The estimates are based on the empirical heat flow-age relations proposed by Polyak and Smirnov (1968) and Hamza and Verma (1969). The use of empirical relations has the advantage that it allows better control on numerical instabilities in harmonic representation. In the work of C&P, mean heat flow were calculated for $5^{\circ} \times 5^{\circ}$ area elements which were subsequently employed in calculating the Legendre coefficients of the spherical harmonic expansion. Two sets of coefficients were calculated: one based exclusively on estimated values for all the grid elements and a second one in which use of estimated values is limited to grid elements devoid of experimental data. The global heat flow maps presented by C&P are derived from these two sets of harmonic coefficients. However, harmonic expansion was carried out only up to degree 12. Hence, the maps derived by C&P display mainly large scale variations in the global conductive heat flow. It also lacks the spatial resolution needed for identifying thermal features associated with local tectonic units.

In spite of such limitations, the maps derived by C&P revealed several important characteristics of global heat flow distribution. Prominent among these are the heat flow anomalies located along the East pacific and South India Ocean ridge systems. High heat flow also occurs along the back-arc regions of the west Pacific and also along the midocean ridge systems. In addition, small scale heat flow anomalies have been identified in the Red Sea area and also in the Persian Gulf and in the Gulf of California. On the other hand, the continents of Asia, Europe, Africa, North America, South America and Australia are identified as areas with heat flux less than 50 mW/m². According to the harmonic analysis of C&P, the mean heat flux of the earth is 59 mW/m².

The work of Pollack et al. (1993), hereafter abbreviated as PH&J, is based largely on the now updated compilation consisting of experimental heat flow values for 20,201 localities. This data set was employed in calculating mean heat flow for a regular grid system composed of $5^{\circ} \times 5^{\circ}$ area elements. However, a careful examination of their procedure reveals that significant modifications were introduced in selecting heat flow values for the grid elements. For example, the use of experimental data and of the estimated values is restricted to areas of old ocean basins and continental margins. In addition, theoretical heat flow values, derived from plate cooling models (McKenzie 1967; Sclater et al. 1980; Stein and Stein 1992) were used for selected segments of ocean ridge areas. This procedure is based on the argument that experimental heat flow data fail to account for heat transfer by supposed hydrothermal circulation in the ocean crust with ages of up to 65 million years. The implicit assumption is that active unconfined hydrothermal systems operate on a regional scale in more than 70% of the oceanic crust.

In our understanding, the practice of using theoretical values as substitute for experimental data is open to criticism, as it is based on assumptions as to the nature of thermal processes at deeper levels in the crust, which is what we are trying to determine in the first place. Another problem with this procedure is that it requires extensive pre-processing of related geological and geophysical information, relevant for heat and mass transfer in a large number of marine tectonic units. In many cases, such supplementary information are not readily available. Detailed geologic mapping of basement structures that control fluid flow beneath ocean basins have not so far been carried out, for obvious limitations in current technological capabilities and because of the costs involved. As a result, the present level of knowledge about the tectonic and structural features of basement layer beneath sediments in oceanic areas is far inferior to that for the crust in continental areas. In spite of the large number of investigations carried out in deep sea areas, much less is known of the deep structure of oceanic crust than its continental counterpart.

At this point, a brief comment on the nature of data sets rejected by PH&J in their analysis of global heat flow is in order. Table 2 provides a summary of the observational data sets that were rejected for the ridge areas of southern oceans. The data have been grouped into $10^{\circ} \times 10^{\circ}$ grid elements. The coordinates of these grid elements are given in columns (2) and (3), means of observed heat flow values in column (4) and number of data points in column (5). Note that the mean values of the rejected data sets for these grid elements fall in the range of 36.9–127 mW/m² for the South Atlantic, 30.9– 97 mW/m² for the Indian Ocean and 18.2-328.6 mW/m² for the Pacific Ocean. These ranges are quite large compared with the uncertainties in oceanic heat flow measurements. It also reveals that the rejected data set includes not only relatively low values (<40 mW/m²) but also values higher than the global average. The criteria for rejection of high heat flow values, which are usually considered as unaffected by down flow of cold fluids, was not discussed explicitly by PH&J. The total number of rejected data for the ridge segments of the southern oceans is 1669, which constitutes nearly 20% of the global ocean heat flow data set.

 Table 2
 Summary of the observational data sets for the southern oceans, rejected by Pollack et al. (1993)

Oceanic region	Longitude	Latitude	Mean heat flow (mW/m ²)	No. of data
Atlantic	-15	-5	53,75	42
	-15	-15	70,93	81
	-5	-15	36,92	18
	-15	-25	79,40	30
	-5	-25	44,95	14
	-15	-35	82,83	23
	-5	-35	69,65	34
	-15	-45	39,80	1
	-15	-55	46,85	2
	-5	-55	127,00	4
Indian	65	-15	41,50	25
	75	-15	53,99	17
	65	-25	86,36	29
	75	-25	82,49	15
	65	-35	43,30	13
	75	-35	47,01	7
	85	-35	67,55	4
	95	-35	30,22	4
	75	-45	49,83	6
	95	-45	64,50	1
	105	-45	95,00	1
	115	-45	35,80	2
	125	-45	37,45	2
	135	-45	54,40	1
	145	-45	97,00	9
	65	-55	63,37	3
	75	-55	55,30	1
Pacific	-115	15	117,86	24
	-105	15	125,11	45
	-95	15	55,11	57
	-115	5	75,34	66
	-105	5	88,99	27
	-95	5	35,97	26
	-85	5	328,61	776
	-115	-5	84,97	12
	-105	-5	124,23	31
	-95	-5	109,61	23
	-125	-15	49,42	22
	-115	-15	111,78	98
	-105	-15	121,45	51
	-125	-25	66,26	8
	-115	-25	167,95	4
	-105	-25	107,90	4
	-125	-45	18,25	2
	-115	-45	86,30	1
	-105	-45	107,75	2
	-95	-45	96,30	1

The data are grouped into $10^{\circ} \times 10^{\circ}$ grid elements

A detailed examination of the database employed by PH&J indicates that results of experimental data were used for only 1,192 grid elements while theoretical heat flow values were used for 835 grid elements. In addition, estimated heat flow values were employed for the remaining 565 grid elements. The large number of grid elements (nearly 32% of the total data set) for which theoretical values were adopted is a characteristic feature of the data set employed by PH&J. Also, in spite of the considerable improvements in the experimental data set, PH&J limited their harmonic representation to degree 12. Hence the map derived in their studies outlines only large scale variations in global heat flow. It depicts most of the continental regions as having mean heat flux of up to 85 mW/m² whereas the ocean ridge systems are depicted as regions with heat flux in excess of 150 mW/m². Another outstanding feature in the map of PH&J is the presence of three major regions in the southern oceans, where heat flux is depicted as having values higher than 200 mW/m^2 . These include ridge areas in the East Pacific, South Mid Atlantic, and South East Indian Oceans. According to the harmonic analysis of PH&J, the value of the first coefficient is 87 mW/m^2 , which implies that the mean heat flow of the earth is nearly 30% higher than the previous estimates.

Though large scale heat flow variations in the global map of PH&J appear at first sight as similar to those outlined in earlier studies a closer examination reveals that significant differences exist. Figure 2 illustrates the differences between global heat flow representations of C&P and PH&J. Note that the magnitudes of heat flow anomalies in the harmonic representation of PH&J are systematically high in both continental and oceanic regions. Such differences may arise as a result of improvements in the database, or a consequence of the widespread use of theoretical heat flow values for oceanic crust. This is a matter of crucial importance in studies of the global thermal fields, but has not received due attention over the last few decades.

Harmonic analysis of conductive heat flow

The problems identified in the harmonic representations of PH&J point to the need for analysis of the global heat flow dataset without recourse to the use of theoretical values. In the present work, we make use of the revised and updated data base set up by Cardoso et al. (2005) and Cardoso (2006). The procedures employed in discretization of this data set are in many aspects similar to those employed in previous studies of C&P and PH&J. Initially mean heat flow values were calculated for $5^{\circ} \times 5^{\circ}$ area elements, based on the available data set. Experimental data are available for 1,239 of such grid elements, out of a total of 2,592, there being 1,353 without data. However, most of grid elements with data are situated in low latitudes and hence its total surface area is higher than that for grid elements without data. Following the procedure of C&P use is made of the empirical predictor in assigning estimated heat flow values to those grid elements for which experimental data are not yet available. The characteristics of the resultant grid system are outlined in the map of Fig. 3 where the red dots indicate area elements for which experimental data are available while the white dots indicate those for which estimated values were employed. As mentioned earlier, theoretical values derived from plate cooling models were not considered in estimating heat flow for the young ocean crust.



Fig. 2 Map of differences in harmonic representations of global heat flow by Pollack et al. (1993) and Chapman and Pollack (1975). The contour values are in units of mW/m^2 . Positive values mean that estimates of Pollack et al. (1993) are higher than the estimates by Chapman and Pollack (1975)



Fig. 3 Grid system used analysis of global heat flow. The *red dots* indicate grid elements for which experimental data are available. The *white dots* indicate grid elements for which estimated values, based on the empirical heat flow-age relation, were used

Subsequent to discretization, fully normalized Legendre coefficients were calculated for 12° spherical harmonic expansion of the homogenized dataset. The basic theory of the method employed in harmonic analysis is well-known (Blakely 1995; Chapman and Bartels 1940). The normalization procedure used in the present work is outlined in Appendix 1. Table 3 lists the new set of coefficients, for harmonic expansion of degree 12. The value of the first coefficient A_{00} and the mean of the individual values of the grid elements are respectively 57.6 and 66.9 mW/m². These values indicate that improvements in the database over the last few decades have not lead to significant changes in the mean global conductive heat flow.

The power spectrum of the harmonic coefficients provides further clues as to the nature of large-scale variations in global heat flow. The variation of the root-mean-square (RMS) amplitude, defined as $\left[\sum_{m} \left(A_{nm}^2 + B_{nm}^2\right)/(2n+1)\right]^{1/2}$, with the degree of harmonic expansion is illustrated in Fig. 4. Note that the amplitudes fall in the rather narrow range of 1-3 mW/m², and the decrease of power with harmonic expansion is relatively smooth. Also shown in Fig. 4 are power spectra determined in the earlier works of C&P and PH&J. Note that the harmonic spectrum of the present work is similar to that reported by C&P, but significantly different from that of PH&J.

The revised sets of harmonic coefficients were employed in deriving new global heat flow maps. The public domain computational package, the Generic mapping tool (GMT) (Wessel and Smith 1998), was used. A number of numerical simulations were carried out using the built-in routines available in GMT, the purpose being to assess the influence of gridding and interpolation procedures in map representations. As an example Fig. 5 shows the global heat flow map based on the new set of Legendre coefficients corresponding to harmonic expansion of degree 12. It reveals that the East Pacific and South East Indian Ocean Ridge systems as well as Japan Sea stand out as oceanic regions with heat flux in the range of 100-150 mW/m². Ridge systems of the Atlantic, Pacific and Indian Oceans also appear as zones of higher than normal heat flux, but the mean values are in the range of 80-100 mW/m². The ocean basins and areas of low angle subduction appear to be characterized by normal heat flux (in the range of 60–80 mW/m²), whereas the central parts of the continental areas of Africa, Asia, North America, South America, Antarctic and Australia seem to be characterized by relatively low heat flux values ($<60 \text{ mW/m}^2$).

The map of Fig. 5 appears, at first sight, to be similar to the one derived in the earlier work by PH&J, but significant differences may easily be noticed on closer examination. For example, the absolute values of conductive heat flow anomalies of the present work are systematically lower

Table 3 Revised set of coefficients (A_{nm} and B_{nm}) for 12° spherical harmonic expansion of conductive heat flow

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4 4 0.250 -4	4.441
5 0 1.081 0	0.000
5 1 -1.116 -0).542
5 2 2.046 0).465
5 3 1.833 -0).643
5 4 -2.900 1	.171
5 5 -1.965 -1	.708
6 0 -1.447 0	0.000
6 1 1.034 1	.398
6 2 1.558 -1	.096
6 3 0.327 -0).354
6 4 -0.793 -0).809
6 5 -0.385 0).437
6 6 0.392 1	.904
7 0 0.886 0	0.000
7 1 0.158 -0).703
7 2 -0.973 0).124
7 3 1.242 -0).409
7 4 0.538 -1	.160
7 5 0.112 1	.171
7 6 -0.568 0).441
7 7 0.780 -0).551
8 0 1.020 0	0.000
8 1 -0.094 1	.534
8 2 1.434 0).237
8 3 -0.548 -0).270
8 4 -0.158 0).190
8 5 0.838 0).560
8 6 1.255 1	.453
8 7 0.555 -0).444
8 8 -0.503 -0).094
9 0 0.261 0).000
9 1 1.183 0	

Table 3 continued

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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	11	-0.129	-0.468
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	0	0.128	0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	1	-0.039	-0.178
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	2	0.033	0.527
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	3	0.808	0.010
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	4	0.091	-0.418
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	5	-0.428	-0.181
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	6	0.749	-0.608
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12 12 -0.535 0.733	12	11	0.119	-0.487
	12	12	-0.535	0.733

than those of PH&J, in both continental and oceanic regions. Also, major positive anomalies have heat flux values in the range of $100-150 \text{ mW/m}^2$, whereas the ones



Fig. 4 Comparison of root-mean-square (rms) amplitudes of the harmonic spectra of global heat flow. The *blue curve* refers to the results of the present work. The *green* and *pink curves* refer to spectra obtained by Chapman and Pollack (1975) and Pollack et al. (1993), respectively



Fig. 5 Global map derived from spherical harmonic expansion to degree 12 of conductive heat flow data. The contour values are in units of mW/m^2

outlined in the earlier work of PH&J have mean heat flux of up to 350 mW/m². Figure 6 illustrates the differences between global heat flow representations of the present work and that of PH&J. The regions of major discrepancies are located in the southern hemisphere along the East Pacific Rise, South Mid Atlantic and South East Indian Ocean ridges. Coincidently, these are also the regions for which PH&J made extensive use of theoretical values derived from plate cooling models. The ridge segments in the northern hemisphere also appear as areas with positive differences. In general, the differences seem to be rather systematic, but clearly more pronounced for the oceanic regions. On the other hand, the differences are found to be much less in continental areas, where theoretical values were not employed.



Fig. 6 Map of differences in harmonic representations of global heat flow by Pollack et al. (1993) and that in the present work. The contour values are in units of mW/m^2 . Positive values mean that estimates of Pollack et al. (1993) are higher than the estimates of the present work

Higher degree harmonic representations

It is a well-known that low degree harmonic representations act as low-pass filters suppressing small-scale variations and enhancing large-scale or regional trends. Obviously, higher degree harmonic expansions are necessary for identifying small-scale variations and also for improving the spatial resolution of large-scale heat flow anomalies. The relation between degree of expansion and spatial resolution may be better understood on the basis of equations used for determination of harmonic coefficients. As demonstrated in Appendix 2 this relation is:

$$m = \frac{\pi}{\Delta\phi} \tag{1}$$

where *m* is the degree of expansion and $\Delta\phi$ the spatial resolution. According to the above equation the resolution associated with 12° harmonic expansion is 15°, which is equivalent to spatial dimensions of approximately 1,600 km in equatorial regions. It is obvious that 12° representations lack the resolution for identifying heat flow anomalies associated with many of the regional tectonic features whose lateral dimensions are less than 1,600 kilometers.

In the present work, the spherical harmonic expansion has been extended to degree 36 as part of an attempt to improve the spatial resolution of the heat flow anomalies. The spatial resolution in this case reaches up to 5° (equivalent to a few hundred kilometers in equatorial regions), which is comparable to the lateral dimensions of such tectonic features as ocean ridges and cratonic areas. However, the choice of higher degree expansion needs to take into consideration the characteristics of data density and its geographic distribution. For 36° expansion, the number of grid elements for which experimental heat flow data is available is slightly less than 50% of the total.



Fig. 7 Global map derived from spherical harmonic expansion to degree 36 of conductive heat flow data. The contour values are in units of mW/m^2

Higher degree expansions would lead to a large number of grid elements with estimated values, making the harmonic representation less reliable. Also, most of the grid elements for which data are available are situated at low latitudes and hence its total surface area is higher than that for grid elements without data. Higher degree expansion would mean a substantial increase in the number grid elements without data at low latitudes. The resulting harmonic representations are likely to be dictated by estimated values rather than by experimental data.

The new set of coefficients, for harmonic expansion of degrees 13–36, is listed in Table 4 of Appendix 3. Note that the harmonic coefficients are independent (orthogonal property of Legendre Polynomials) and hence the set in Table 4 is actually a complement to that provided in Table 3, for harmonic expansions of degrees 1–12.

The set of global heat flow maps derived from coefficients corresponding to harmonic expansions of degrees 1 to 36 reveal that the improvement in spatial resolution of heat flow anomalies is substantial for low harmonics, reaching up to degree 12. In the range corresponding to degrees higher than 12 the improvement is slow but steady. Calculation of RMS amplitudes indicates that the contribution of higher harmonics is approximately 10%. The global heat flow map derived for harmonic expansion of degree 36 is presented in Fig. 7. The outstanding feature of this map is its relatively better resolution, which has allowed significant improvements in outlining the major heat flow anomalies in both continental and oceanic regions. This can easily be seen by comparing the map of Fig. 7 with the map derived from harmonic representation of degree 12 (Fig. 5). Prominent examples are the positive anomalies in East Pacific, South Indian Ocean, and the back-arc regions of the west Pacific. Other examples include the anomalies associated with the ocean ridges in the Atlantic, Pacific, and Indian Oceans where heat flow is higher than normal (generally in the range of 80-100 mW/ m²). Improvements can also be seen in delimiting low heat flux (<60 mW/m²) regions in the central parts of the continental areas of Africa, Asia, North America, South America, Antarctic, and Australia.

Discussion

The results obtained in the present work reveal that harmonic representation based on conductive heat flow lead to global heat flow maps that are substantially different from those presented by PH&J. Such differences have potential implications for studies of large-scale variations of heat flow of the earth and also in estimates of the rates of global heat loss. However, lack of direct evidences about the details of hydrothermal processes in the ocean crust makes it difficult to decide which of the representation provides a better approximation of the true heat flow field of the earth. In this context, the harmonic representation of conductive heat flow may be considered as an alternative providing minimum estimates of global heat loss. Nevertheless, the implications of this representation need to be tested against independent lines of evidence concerning the thermal state of the earth's interior. In trying to address this problem we focus the discussion here on the following items that may provide potentially useful information:

- Comparative analysis of large-scale features discernible in harmonic and numerical representations of regional heat flow; and
- 2. Independence of the harmonic coefficients and its consequence in low degree representations of heat flow in the oceanic crust.

Comparison between numerical and harmonic representations

Large-scale trends discernible in numerical representations of regional heat flow provide a convenient means of verifying features identified in harmonic representations. Continental areas of Australia and South America were selected for such comparative studies. These are relatively small continents whose regional heat flow fields are relatively well-known (Cull 1982; Hamza and Muñoz 1996; Hamza et al. 2005). In addition, heat flow in upper crustal layers of these continental regions is free of the eventual perturbing effects of hydrothermal circulation of ocean waters. The numerical representation of the regional heat

Fig. 8 a Numerical representation of regional heat flow in the Australian continental region (Cull 1982; Cardoso and Hamza 2005). b Regional heat flow map of the Australian continental region, derived from spherical harmonic expansion to degree 12 of Pollack et al. (1993). c Regional heat flow map of the Australian continental region, derived from spherical harmonic expansion to degree 36 of the present work



flow field of Australia, presented in Fig. 8a, indicates a north-south trending belt of high heat flow in its central part and low heat flow areas in the western and eastern parts (Cull and Denham 1979; Cardoso and Hamza 2005). Regional heat flow map based on harmonic representations of PH&J, presented in Fig. 8b, reveal a completely different pattern, pointing to an east–west trending low to normal heat flow. On the other hand, the map derived from harmonic coefficients of the present work (Fig. 8c) is found

to be capable of outlining large-scale features similar to the ones encountered in the numerical representation (Fig. 8a).

The numerical representation of the heat flow field of South American continent is illustrated in the map of Fig. 9a. It reveals that heat flow is relatively high in areas along the Andean belt and also in the Patagonian platform. The regional heat flow maps based on harmonic representations of PH&J and of the present work are illustrated in Fig. 9b, c, respectively. Note that the

Fig. 9 a Numerical representation of regional heat flow in the South American continental region (Hamza et al. 2005; Cardoso and Hamza 2005). **b** Regional heat flow map of the South American continental region, derived from spherical harmonic expansion to degree 12 of Pollack et al. (1993). **c** Regional heat flow map of the South American continental region, derived from spherical harmonic expansion to degree 36 of the present work







Fig. 10 a Regional heat flow map of the Equatorial region of the Atlantic Ocean, derived from the spherical harmonic expansion to degree 12 of Pollack et al. (1993). c Regional heat flow map of the

Equatorial region of the Atlantic Ocean, derived from the spherical harmonic expansion to degree 36 of the present work

characteristics of regional anomalies of Fig. 9b are considerably different from those present in the map of Fig. 9a. On the other hand the regional features present in harmonic representation of the present work (Fig. 9c) are quite similar to those of the numerical representation (Fig. 9a).

Independence of harmonic coefficients and consequences for low degree representations

The coefficients derived in spherical harmonic analysis are independent (property of orthogonal polynomials) for any particular data set. This is usually considered an important advantage in data analysis (Bevington 1969), but it also has undesirable consequences when modifications are necessary for subsets of data. This can easily be understood by considering the relevant expressions for the harmonic coefficients (see Appendix 1). In the case of discrete data sets the equations for the coefficients are recast as:

$$A_{nm} = \frac{1}{4\pi} \sum_{\phi=0}^{2\pi} \sum_{\theta=0}^{\pi} \overline{q}(\theta,\phi) \cos m\phi \sin \theta P_{nm}(\cos \theta) \Delta \phi \Delta \theta$$
(2)

$$B_{nm} = \frac{1}{4\pi} \sum_{\phi=0}^{2\pi} \sum_{\theta=0}^{\pi} \overline{q}(\theta,\phi) \sin m\phi \sin \theta P_{nm}(\cos \theta) \Delta \phi \Delta \theta \quad (3)$$

It is apparent that the values of A_{nm} and B_{nm} depends on the integral over the mean values $q(\theta, \phi)$ of the grid elements. Consequently, modifications in the dataset for any particular region lead to significant alterations in the entire set of coefficients.

In the work of PH&J, heat flux values for the ridge segments and most of the young ocean crust were upgraded, in an attempt to account for the supposed effect of regional-scale convection heat transfer. However, such upgrading has a direct effect not only on the representation of heat flow in the ocean ridge areas but also that for the remaining regions of the earth, where convective heat transfer is practically insignificant or altogether absent. As an illustrative example consider the heat flow field for the equatorial region of the Atlantic Ocean. The relevant regional heat flow map, derived from the harmonic coefficients of PH&J is presented in Fig. 10a. Note the presence of a rather very broad heat flow anomaly (with values in excess of 80 mW/m²) over much of the oceanic crust in the central Atlantic region. Such high heat flow anomalies are incompatible with the experimental heat flow data for this region (Sclater et al. 1980; Cardoso and Hamza 2006). The unavoidable conclusion is that upgrading heat flow in ridge areas has lead to overestimates of heat flow in older segments of the ocean crust where perturbing effects of hydrothermal circulation is negligible or altogether absent.

For comparison purposes we present in Fig. 10b the regional heat flow map of the same region derived from the new set of coefficients for the 36° harmonic expansion of the present work. Note that heat flux in excess of 80 mW/m^2 is encountered only along a narrow belt that encompasses the axial region of the mid Atlantic ridge. The off-ridge parts of the oceanic regions and

continental margins have heat flux values of less than 60 mW/m^2 . Thus the overall picture is in much better agreement with the experimental data set and the mean values calculated by Sclater et al. (1980) and Cardoso and Hamza (2006).

Conclusions

Harmonic analysis, with due emphasis on experimental heat flow values, has lead to results that are significantly different from that presented in the earlier work of PH&J. Our results are compatible with the characteristics of crustal thermal fields outlined in regional studies. The mean global heat flow is found to fall in the range of 56–67 mW/m². These estimates are markedly lower than the global mean of 87 mW/m² calculated by PH&J. On the other hand, the range is in reasonable agreement with the mean value of 63 mW/m², determined recently by Hofmeister and Criss (2005) on the basis of geochemical arguments.

The results obtained also allow new estimates of global heat loss. The values of global heat loss based on the first coefficient (A_{00}) and integration of binned data are respectively 28.6 and 34.1 TW. These estimates are found to bracket the value proposed by Hofmeister and Criss (2005). Again, our estimates are found to be significantly lower than the value of 44.2 TW obtained by PH&J.

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Appendix 1

Harmonic coefficients and the normalization procedure

The harmonic representation of heat flow (q) in near surface layers is usually expressed as:

$$q(\theta,\phi) = \sum_{n=0}^{N} \sum_{m=0}^{n} [A_{nm} \cos\left(m\phi\right) + B_{nm} \sin\left(m\phi\right)] P'_{nm}(\cos\theta)$$
(4)

where ϕ is the longitude $\theta = 90 - \psi$, is the colatitude, P'_{nm} (cos θ) is the associated Legendre function that is fully normalized and A_{nm} and B_{nm} the coefficients of the harmonic expansion. The expression for evaluation of P'_{nm} is:

$$P_{nm} = \frac{P_{nm}}{\sqrt{K_n^m}} \tag{5}$$

where P_{nm} is the associated Legendre function given by:

$$P_{nm}(\cos\theta) = \frac{\sin^{m}\theta}{2^{n}} \sum_{t=0}^{lnt} \frac{(-1)^{t}(2n-2t)!}{t!(n-t)!(n-m-2t)!} \cos^{(n-m-2t)}\theta$$
(6)

and

$$K_n^m = \frac{1}{H(2n+1)} \frac{(n+m)!}{(n-m)!}, \begin{cases} \text{if } m = 0 \Rightarrow H = 0\\ \text{if } m \neq 0 \Rightarrow H = 2 \end{cases}$$
(7)

In Eq. (6) Int[(n-m)/2] refers to the largest integer that is lower than (n-m)/2.

Full normalization of associated Legendre functions (P_{nm}) requires that the following equations be satisfied:

$$\int_{0}^{2\pi} \int_{0}^{\pi} \left[P'_{nm}(\cos\theta) \sin(m\phi) \right]^2 \sin\theta \, \mathrm{d}\theta \, \mathrm{d}\phi = 4\pi \tag{8a}$$

$$\int_{0}^{2\pi} \int_{0}^{\pi} \left[P'_{nm}(\cos\theta) \cos(m\phi) \right]^2 \sin\theta \, \mathrm{d}\theta \, \mathrm{d}\phi = 4\pi \tag{8b}$$

The coefficients A_{nm} and B_{nm} are evaluated by fitting the harmonic expansion to the set of experimental data, which are the heat flow values (q) and their respective geographic coordinates (ϕ and θ).

Appendix 2

Relation between degree of harmonic expansion and spatial resolution

A discrete distribution of *N* data points over the surface of the earth at a specific latitude (θ_0) and spaced at an angular distance of $\Delta \Phi$ follow the relation:

$$N = \frac{2\pi}{\Delta\phi} \tag{9}$$

A function $\overline{q}(\theta_0, \phi)$ which represents heat flow at a specific latitude θ_0 , but continuous in ϕ between 0 and 2π may be represented as Fourier sine series:

$$\overline{q}(\theta_o,\phi) = \sum_{m=0}^{\infty} (a_m(\theta_o)\cos m\phi + b_m(\theta_o)\sin m\phi)$$
(10)

The coefficients $a_m(\theta_0)$ and $b_m(\theta_0)$ are calculated using discretized values experimental heat flow $(q(\phi))$ uniformly

distributed over the surface of the earth with angular spacing of $\Delta \varphi$. The expressions for the calculation of the coefficients are:

$$a_m(\theta_0) = \frac{2}{N} \sum_{t=1}^N q_t(\phi) \cos\left(\frac{2\pi mt}{N}\right) \tag{11}$$

$$b_m(\theta_0) = \frac{2}{N} \sum_{t=1}^{N} q_t(\phi) \sin\left(\frac{2\pi mt}{N}\right)$$
(12)

Obviously when $\overline{q}(\phi) = q(\phi)$ Eq. (10) will represent the exact value of the discretized heat flux. This condition allows determination of the "*m*" to be used in the expansion. The result may be obtained as follows:

1. Substitute Eqs. (11) and (12) in Eq. (10):

$$\overline{q}(\theta_0, \phi) = \sum_{m=0}^{\infty} \left(\frac{2}{N} \sum_{t=1}^{N} q_t(\phi) \cos\left(\frac{2\pi m t}{N}\right) \cos(m\phi) + \frac{2}{N} \sum_{t=1}^{N} q_t(\phi) \sin\left(\frac{2\pi m t}{N}\right) \sin(m\phi) \right)$$
(13)

2. Substitute Eq. (9) in Eq. (13):

$$\overline{q}(\theta_0, \phi) = \frac{2}{N} \sum_{m=0}^{\infty} \left(\sum_{t=1}^{N} q_t(\phi) \cos(mt\Delta\phi) \cos(m\phi) + \sum_{t=1}^{N} q_t(\phi) \sin(mt\Delta\phi) \sin(m\phi) \right)$$
(14)

3. The longitude " ϕ_k " may be represented as $\phi_i = k\Delta\phi$, where *k* is a natural number, so after substitution we have:

$$\begin{aligned} \overline{q}_k(\theta_0, k\Delta\phi) &= \frac{2}{N} \sum_{m=0}^{\infty} \left(\sum_{t=1}^{N} q_t(k\Delta\phi) \cos(mt\Delta\phi) \cos(mk\Delta\phi) \right. \\ &+ \left. \sum_{t=1}^{N} q_t(k\Delta\phi) \sin(mt\Delta\phi) \sin(mk\Delta\phi) \right) \end{aligned}$$

4. By the principle of orthogonality, the product $\cos(mt\Delta\phi)\cos(mk\Delta\phi)$ is non-zero only for t = k. Thus all the summation terms become zero except for the term "k", and so we have:

$$\overline{q}_{k}(\theta_{0}, k\Delta\phi) = \frac{2}{N} \sum_{m=0}^{\infty} (q_{k}(k\Delta\phi)\cos(mk\Delta\phi)\cos(mk\Delta\phi) + q_{k}(k\Delta\phi)\sin(mt\Delta\phi)\sin(mk\Delta\phi))$$

$$\overline{q}_{k}(\theta_{0}, k\Delta\phi) = \frac{2}{N} \sum_{m=0}^{\infty} (q_{k}(k\Delta\phi) \cos^{2}(mk\Delta\phi) + q_{k}(k\Delta\phi) \sin^{2}(mt\Delta\phi))$$

which, upon simplification leads to:

$$\overline{q}_k(\theta_0, k\Delta\phi) = \frac{2}{N} \sum_{m=0}^{\infty} q_k(k\Delta\phi)$$

5. Applying the property of summation:

$$\overline{q}_k(\theta_0, k\Delta\phi) = \frac{2}{N} m q_k(k\Delta\phi)$$

6. As $\overline{q}_k(\theta_0, k\Delta\phi)$ must be equal to q_k ($k\Delta\phi$) we have: $1 = \frac{2}{N}m$ which, after substitution of Eq. (9), leads to: $m = \frac{\pi}{\Delta\phi}$

Appendix 3

Table 4.

Fable 4	Coefficients	for	harmonic	expansion	of degree	e 36
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n	m	Anm	Bnm
13	0	-0.113	0.000
13	1	0.079	0.271
13	2	0.043	0.360
13	3	0.022	0.230
13	4	0.068	0.004
13	5	0.062	-0.263
13	6	-0.414	-0.207
13	7	0.123	-0.122
13	8	-0.054	0.481
13	9	0.110	0.344
13	10	0.086	-0.096
13	11	-0.223	-0.185
13	12	-0.119	0.578
13	13	0.011	-0.024
14	0	0.038	0.000
14	1	-0.088	0.264
14	2	-0.007	0.044
14	3	0.300	0.146
14	4	0.051	-0.341
14	5	0.185	-0.272
14	6	-0.284	-0.181
14	7	0.051	0.062
14	8	-0.041	0.159
14	9	-0.027	0.135
14	10	0.118	-0.314
14	11	0.053	-0.074
14	12	-0.306	0.159
14	13	0.107	0.070
14	14	0.026	-0.130
15	0	0.200	0.000
15	1	-0.057	0.097
15	2	0.223	-0.391
15	3	0.156	0.069

Table 4 continued

Table 4	continued			Table 4 continued			
n	т	Anm	Bnm	n	т	Anm	Bnm
15	4	-0.092	-0.404	18	1	-0.121	-0.148
15	5	0.046	-0.120	18	2	-0.105	0.035
15	6	-0.131	-0.245	18	3	-0.064	-0.114
15	7	-0.067	0.255	18	4	-0.101	0.225
15	8	-0.028	0.087	18	5	0.029	0.023
15	9	-0.074	0.199	18	6	0.080	0.173
15	10	-0.103	-0.135	18	7	0.035	-0.097
15	11	-0.093	0.162	18	8	-0.030	-0.089
15	12	-0.012	0.296	18	9	-0.166	-0.175
15	13	-0.062	0.260	18	10	-0.074	0.153
15	14	-0.010	-0.291	18	11	-0.218	0.134
15	15	-0.390	0.226	18	12	-0.008	-0.162
16	0	0.322	0.000	18	13	0.154	-0.374
16	1	0.081	-0.114	18	14	-0.101	0.109
16	2	0.172	-0.200	18	15	-0.314	0.116
16	3	-0.109	0.065	18	16	0.365	-0.012
16	4	0.001	-0.099	18	17	0.316	-0.031
16	5	-0.127	-0.001	18	18	0.063	-0.142
16	6	0.009	0.039	19	0	0.007	0.000
16	7	-0.300	0.196	19	1	-0.002	0.016
16	8	0.157	-0.051	19	2	-0.103	0.087
16	9	0.118	-0.135	19	3	-0.034	0.207
16	10	0.227	0.098	19	4	-0.177	0.140
16	11	-0.189	0.283	19	5	0.093	0.032
16	12	-0.006	0.170	19	6	0.023	-0.087
16	13	0.129	-0.020	19	7	-0.058	-0.208
16	14	-0.173	-0.082	19	8	-0.132	-0.125
16	15	-0.227	-0.275	19	9	-0.066	0.045
16	16	-0.062	0.185	19	10	-0.156	0.126
17	0	-0.030	0.000	19	11	-0.069	0.197
17	1	-0.011	-0.286	19	12	0.006	-0.015
17	2	-0.135	0.118	19	13	0.264	-0.035
17	3	-0.117	-0.121	19	14	-0.084	-0.043
17	4	0.154	0.262	19	15	-0.034	0.097
17	5	-0.139	0.066	19	16	0.084	-0.123
17	6	0.138	0.354	19	17	0.032	-0.203
17	7	-0.215	0.009	19	18	0.191	-0.301
17	8	0.161	-0.167	19	19	-0.278	0.013
17	9	0.078	-0.443	20	0	0.116	0.000
17	10	0.246	0.317	20	1	0.062	0.008
17	11	-0.171	0.119	20	2	-0.075	0.218
17	12	-0.015	0.119	20	3	0.124	0.232
17	13	0.197	-0.363	20	4	0.180	0.227
17	14	-0.065	-0.013	20	5	0.111	-0.004
17	15	-0.053	0.088	20	6	0.025	-0.052
17	16	0.048	0.212	20	7	-0.072	-0.176
17	17	0.462	0.013	20	8	-0.131	-0.162
18	0	-0.093	0.000	20	9	0.029	0.053
-	~		5.000	~	~	~~~~~	0.000

Table 4 continued

	Table 4	continued			Table 4	continued		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	n	т	Anm	Bnm	n	т	Anm	Bnm
20110.0570.00822160.382-0.02320120.1250.0922217-0.1030.04420130.0216-0.1352218-0.1820.442014-0.054-0.09922190.544-0.03220160.177-0.2432221-0.0640.02320170.085-0.19222-0.031-0.0922018-0.382-0.4112300.2030.0002019-0.122-0.1882310.025-0.053210-0.1110.00233-0.033-0.033211-0.0840.159234-0.051-0.2322130.139-0.055236-0.239-0.0162130.127-0.150238-0.0330.0612140.2290.099237-0.0490.0662150.127-0.1502313-0.0330.0182110-0.0440.80823110.1250.175219-0.0440.8082312-0.147-0.24421100.01623150.0930.09821130.088-0.023150.0930.0982114-0.272-0.23150.093<	20	10	-0.149	0.262	22	15	0.017	-0.064
2012 0.125 0.092 22 17 -0.103 0.044 2013 0.216 -0.135 2218 -0.163 0.043 2014 -0.054 -0.099 2219 0.544 -0.043 2015 0.018 0.103 2220 0.0685 0.033 2016 0.177 -0.243 2221 -0.064 0.023 2018 -0.382 -0.411 230 0.023 -0.085 2020 0.122 0.183 232 0.107 -0.223 210 -0.111 0.000 233 -0.051 -0.051 212 0.033 0.006 235 -0.115 -0.016 213 0.127 -0.059 237 -0.049 0.066 215 0.127 -0.150 238 -0.033 0.016 215 0.127 -0.050 2310 0.0448 -0.168 217 0.028 -0.037 2310 0.0448 -0.168 218 -0.039 0.038 2311 0.125 0.172 219 -0.044 0.080 2312 -0.147 -0.424 2110 -0.144 0.089 2314 -0.168 0.099 2113 0.086 0.099 2314 -0.147 0.044 2114 <td>20</td> <td>11</td> <td>0.057</td> <td>0.008</td> <td>22</td> <td>16</td> <td>0.382</td> <td>-0.020</td>	20	11	0.057	0.008	22	16	0.382	-0.020
20130.216 -0.135 2218 -0.182 0.1432014 -0.054 -0.099 22190.544 -0.042 20150.0180.10322220.0850.01420160.177 -0.243 2221 -0.064 0.00520170.085 -0.139 2222 -0.011 -0.023 2019 -0.122 -0.18 2310.0230.00020200.1220.1832310.025 -0.085 2120.0840.159234 -0.051 -0.233 2120.0330.006233 -0.035 -0.061 2130.139 -0.035 236 -0.239 -0.166 2140.028 -0.037 2310 0.048 -0.661 2170.028 -0.037 2311 0.166 0.075 -0.061 239 0.097 0.133 2170.028 -0.037 2311 0.125 0.075 0.061 2312 -0.147 -0.242 2110 -0.044 0.0902313 -0.066 0.098 21 1.098 0.038 0.098 21130.0860.0282314 0.196 0.044 0.099 0.170 0.027 2114 -0.272 -0.024 23	20	12	0.125	0.092	22	17	-0.103	0.048
2014 -0.054 -0.099 2219 0.544 -0.042 2015 0.018 0.013 2220 0.065 0.014 2016 0.177 -0.232 22 22 -0.031 -0.062 2017 0.085 -0.139 2222 -0.031 -0.093 2019 -0.122 -0.188 231 0.025 -0.085 2020 0.122 0.183 232 0.107 -0.227 210 -0.111 0.000 233 -0.051 -0.051 211 -0.084 0.159 234 -0.051 -0.051 212 0.033 0.006 235 -0.115 0.006 213 0.139 -0.35 236 -0.049 0.066 215 0.127 -0.150 238 -0.033 0.016 216 0.075 -0.061 2310 0.048 -0.164 217 0.028 -0.077 2310 0.048 -0.061 218 -0.308 0.038 2311 0.125 0.172 219 -0.044 0.080 2314 0.096 0.048 2110 -0.144 0.167 2313 -0.086 0.098 2113 0.082 0.06 2316 0.447 0.168 2114 0	20	13	0.216	-0.135	22	18	-0.182	0.143
20150.0180.10322200.0850.31420160.177 -0.243 2221 -0.064 0.02520170.085 -0.139 2221 -0.031 -0.092 2018 -0.382 -0.411 2300.2030.00020200.122 -0.158 2310.025 -0.083 21200.0120.0830.06233 -0.051 -0.232 211 -0.084 0.159234 -0.051 -0.332 2120.0330.006235 -0.115 0.0162130.139 -0.055 236 -0.239 -0.166 2140.027 -0.150 238 -0.033 0.0162150.127 -0.150 238 -0.033 0.0162160.075 -0.061 2390.0970.1332170.028 -0.037 212 -0.147 -0.242 219 -0.044 0.08023110.1250.172219 -0.044 0.08023140.196 -0.245 21130.088 -0.028 21160.4270.1062114 -0.272 -0.024 2317 -0.186 0.19721150.0490.0092318 -0.141 <td>20</td> <td>14</td> <td>-0.054</td> <td>-0.099</td> <td>22</td> <td>19</td> <td>0.544</td> <td>-0.042</td>	20	14	-0.054	-0.099	22	19	0.544	-0.042
20160.177-0.2432221-0.0640.02520170.085-0.1392222-0.031-0.0922018-0.382-0.1112300.2030.000200.122-0.1882310.025-0.085210-0.1110.000233-0.035-0.055211-0.0840.159234-0.051-0.2362120.0330.006235-0.1150.1062130.139-0.055236-0.239-0.0162140.2290.099237-0.0490.0672150.127-0.150238-0.0330.0182170.028-0.03723100.048-0.168218-0.0380.03823110.1250.173219-0.0440.0802312-0.147-0.2422110-0.1040.1572313-0.0860.09821120.098-0.02223160.04270.00821130.0820.26623160.4270.0082114-0.272-0.02423190.1700.06721150.0360.0952323-0.1840.10121160.3220.01623 <td< td=""><td>20</td><td>15</td><td>0.018</td><td>0.103</td><td>22</td><td>20</td><td>0.085</td><td>0.314</td></td<>	20	15	0.018	0.103	22	20	0.085	0.314
20170.085 -0.139 2222 -0.031 -0.093 2018 -0.382 -0.411 2300.0050.00520200.1220.1882320.107 -0.227 210 -0.111 0.000233 -0.035 -0.035 211 -0.084 0.159234 -0.035 -0.035 2120.0330.006235 -0.115 -0.036 2130.139 -0.035 236 -0.239 -0.166 2140.2290.099237 -0.049 0.066 2170.028 -0.037 2310 0.048 -0.136 2170.028 -0.037 2311 0.125 0.177 2170.0440.0802312 -0.147 -0.242 2110 -0.144 0.157 2313 -0.086 0.098 21130.0820.2316 0.427 0.168 2114 -0.272 -0.24 2317 -0.186 0.199 21150.0040.0092318 -0.147 -0.242 2114 -0.272 -0.24 2317 -0.186 0.199 21150.0040.0092318 -0.147 -0.066 21160.3220.062320 0.299 </td <td>20</td> <td>16</td> <td>0.177</td> <td>-0.243</td> <td>22</td> <td>21</td> <td>-0.064</td> <td>0.029</td>	20	16	0.177	-0.243	22	21	-0.064	0.029
2018 -0.382 -0.411 230 0.203 0.000 2019 -0.122 -0.158 231 0.025 -0.68 210 -0.111 0.000 233 -0.035 -0.035 211 -0.044 0.159 234 -0.051 -0.232 212 0.033 0.066 235 -0.115 0.016 213 0.139 -0.035 236 -0.239 -0.166 214 0.229 0.099 237 -0.049 0.066 215 0.177 -0.051 238 -0.033 0.018 216 0.075 -0.061 239 0.097 0.133 217 0.028 -0.037 2311 0.148 -0.166 218 -0.044 0.080 2312 -0.147 -0.242 2110 -0.044 0.080 2312 -0.147 -0.242 2111 0.183 -0.28 2314 0.096 0.095 2113 0.082 0.266 2316 0.026 0.016 2114 -0.072 -0.024 2317 -0.186 0.0192 2115 0.004 0.099 232320 0.269 0.166 2114 -0.027 -0.024 2320 0.076 0.072 2116 </td <td>20</td> <td>17</td> <td>0.085</td> <td>-0.139</td> <td>22</td> <td>22</td> <td>-0.031</td> <td>-0.093</td>	20	17	0.085	-0.139	22	22	-0.031	-0.093
2019 -0.122 -0.158 231 0.025 -0.085 2020 0.0122 0.183 232 0.107 -0.223 210 -0.111 0.000 233 -0.055 -0.055 211 -0.084 0.159 234 -0.051 -0.236 212 0.033 0.006 235 -0.115 0.106 213 0.139 -0.35 236 -0.239 -0.166 215 0.077 -0.061 238 -0.033 0.097 216 0.075 -0.061 239 0.097 0.133 217 0.028 -0.37 2310 0.048 -0.166 218 -0.308 0.038 2311 0.125 0.175 219 -0.044 0.080 2312 -0.147 -0.242 2110 -0.044 0.080 2312 -0.147 -0.242 2111 0.183 -0.26 2316 0.427 0.106 2112 0.098 -0.022 2316 0.427 0.106 2113 0.082 0.206 2316 0.427 0.106 2114 -0.272 -0.024 2317 -0.186 0.191 2115 0.004 0.099 2322 -0.073 0.125 2118 0.04	20	18	-0.382	-0.411	23	0	0.203	0.000
2020 0.122 0.183 232 0.107 -0.227 210 -0.0111 0.000 233 -0.055 -0.053 211 -0.084 0.159 234 -0.051 -0.236 212 0.033 0.006 235 -0.115 0.016 213 0.139 -0.35 236 -0.239 -0.166 214 0.229 0.099 237 -0.049 0.066 215 0.127 -0.150 238 -0.031 0.018 216 0.075 -0.061 239 0.097 0.130 217 0.028 -0.037 2310 0.048 -0.164 218 -0.308 0.038 2311 0.1425 0.173 219 -0.044 0.080 2312 -0.147 -0.242 2110 -0.104 0.157 2313 -0.086 0.098 2112 0.098 -0.022 2315 0.093 0.099 2113 0.082 0.206 2316 0.427 0.108 2114 -0.772 -0.024 2317 -0.186 0.149 2115 0.004 0.009 2320 0.269 -0.192 2114 0.272 -0.242 2 0.017 0.066 2116 0.322 0	20	19	-0.122	-0.158	23	1	0.025	-0.085
210 -0.111 0.000233 -0.035 -0.035 211 -0.084 0.159234 -0.051 -0.232 2120.0330.006235 -0.115 0.0062130.139 -0.035 236 -0.239 -0.166 2140.2290.099237 -0.049 0.0672150.127 -0.150 238 -0.037 0.0182160.075 -0.061 2390.0970.1332170.028 -0.037 23100.048 -0.166 218 -0.036 0.03823110.1250.173219 -0.044 0.0802313 -0.086 0.0982110 -0.104 0.1572313 -0.086 0.09821110.183 -0.28 23140.196 -0.244 21120.098 -0.022 23150.0930.09521130.0820.02223160.4270.1662114 -0.272 -0.024 2317 -0.186 0.19921150.0040.0092318 -0.147 0.16621160.3220.01623200.269 -0.192 21190.0020.12123200.269 -0.192 <tr< td=""><td>20</td><td>20</td><td>0.122</td><td>0.183</td><td>23</td><td>2</td><td>0.107</td><td>-0.227</td></tr<>	20	20	0.122	0.183	23	2	0.107	-0.227
211 -0.084 0.159 23 4 -0.051 -0.236 21 2 0.033 0.006 23 5 -0.115 0.016 21 3 0.129 -0.035 23 6 -0.239 -0.166 21 4 0.229 0.099 23 7 -0.049 0.066 21 5 0.127 -0.150 23 8 -0.033 0.018 21 6 0.075 -0.061 23 9 0.097 0.133 21 7 0.028 -0.037 23 10 0.048 -0.147 21 7 0.028 -0.037 23 11 0.125 0.175 21 9 -0.044 0.080 23 112 -0.147 -0.242 21 10 -0.164 0.187 23 13 -0.066 0.098 21 11 0.183 -0.208 23 14 0.196 -0.244 21 12 0.098 -0.022 23 15 0.093 0.095 21 13 0.082 0.066 23 16 0.427 0.166 21 14 -0.272 -0.24 23 17 -0.186 0.192 21 15 0.004 0.099 23 21 -0.086 0.142 21 16 0.322 0.016 23 19 0.170 0.066 21 17 -0.211 -0.026 0.24 </td <td>21</td> <td>0</td> <td>-0.111</td> <td>0.000</td> <td>23</td> <td>3</td> <td>-0.035</td> <td>-0.053</td>	21	0	-0.111	0.000	23	3	-0.035	-0.053
212 0.033 0.006 235 -0.115 0.106 213 0.139 -0.035 236 -0.239 -0.16 214 0.229 0.099 237 -0.049 0.067 215 0.127 -0.150 238 -0.033 0.018 216 0.075 -0.061 239 0.097 0.130 217 0.028 -0.037 2310 0.048 -0.162 218 -0.308 0.038 2311 0.125 0.173 219 -0.044 0.080 2312 -0.147 -0.243 2110 -0.104 0.157 2313 -0.086 0.098 2111 0.183 -0.208 2314 0.196 -0.249 2113 0.082 0.206 2316 0.427 0.106 2114 -0.272 -0.024 2317 -0.186 0.191 2115 0.004 0.009 2318 -0.144 -0.066 2116 0.322 0.016 2319 0.170 0.067 2117 -0.211 -0.069 2320 0.269 -0.192 2118 0.041 0.029 2323 -0.181 -0.166 2119 0.002 0.121 2323 -0.181 -0.057 2110 0	21	1	-0.084	0.159	23	4	-0.051	-0.236
213 0.139 -0.035 23 6 -0.239 -0.166 21 4 0.229 0.099 23 7 -0.049 0.067 21 5 0.127 -0.150 23 8 -0.033 0.018 21 6 0.075 -0.061 23 9 0.097 0.133 21 7 0.028 -0.037 23 10 0.048 -0.168 21 8 -0.308 0.038 23 11 0.125 0.177 21 9 -0.044 0.080 23 12 -0.147 -0.243 21 10 -0.104 0.157 23 13 -0.086 0.098 21 11 0.183 -0.228 23 14 0.196 -0.249 21 12 0.098 -0.022 23 15 0.093 0.099 21 14 -0.272 -0.024 23 17 -0.186 0.191 21 15 0.004 0.009 23 18 -0.144 -0.106 21 16 0.322 0.016 23 19 0.170 0.066 21 18 0.041 0.029 23 21 -0.086 0.142 21 19 0.002 0.121 23 22 -0.073 0.122 21 19 0.022 0.121 23 22 -0.073 0.022 21 19 0.002 0.122 <td>21</td> <td>2</td> <td>0.033</td> <td>0.006</td> <td>23</td> <td>5</td> <td>-0.115</td> <td>0.106</td>	21	2	0.033	0.006	23	5	-0.115	0.106
214 0.229 0.099 23 7 -0.049 0.067 215 0.127 -0.150 23 8 -0.033 0.018 216 0.075 -0.061 23 9 0.097 0.133 217 0.028 -0.037 23 10 0.048 -0.168 218 -0.308 0.038 23 11 0.125 0.173 219 -0.044 0.080 23 12 -0.147 -0.242 2110 -0.104 0.157 23 13 -0.086 0.098 2111 0.183 -0.208 23 14 0.196 -0.245 2112 0.098 -0.022 23 15 0.093 0.099 2113 0.082 0.206 23 16 0.427 0.168 2114 -0.272 -0.024 23 17 -0.186 0.191 2115 0.004 0.099 23 18 -0.144 -0.166 2117 -0.211 -0.692 23 20 0.269 -0.196 2118 0.041 0.029 23 23 -0.181 -0.166 2119 0.002 0.121 23 22 -0.073 0.125 2120 -0.366 0.095 23 23 -0.181 -0.162 2119 0.002 0.122 24 4	21	3	0.139	-0.035	23	6	-0.239	-0.166
215 0.127 -0.150 238 -0.033 0.018 216 0.075 -0.061 239 0.097 0.136 217 0.028 -0.037 2310 0.048 -0.168 218 -0.308 0.038 2311 0.125 0.177 219 -0.044 0.080 2312 -0.147 -0.242 2110 -0.104 0.157 2313 -0.086 0.098 2112 0.098 -0.022 2315 0.093 0.099 2113 0.082 0.206 2316 0.427 0.108 2114 -0.772 -0.024 2317 -0.186 0.191 2115 0.004 0.009 2318 -0.144 -0.106 2117 -0.211 -0.069 2320 0.269 -0.196 2118 0.041 0.029 2321 -0.086 0.144 2119 0.002 0.121 2322 -0.073 0.125 2120 -0.036 0.095 2323 -0.181 -0.169 2118 0.041 0.029 2323 -0.181 -0.05 2120 0.036 0.095 2323 -0.181 -0.060 2121 0.226 0.12 24 0 0.175 0.000 220 <t< td=""><td>21</td><td>4</td><td>0.229</td><td>0.099</td><td>23</td><td>7</td><td>-0.049</td><td>0.067</td></t<>	21	4	0.229	0.099	23	7	-0.049	0.067
2160.075-0.0612390.0970.1302170.028-0.03723100.048-0.166218-0.3080.03823110.1250.173219-0.0440.0802312-0.147-0.2422110-0.1040.1572313-0.0860.09821110.183-0.20823140.196-0.24521120.098-0.02223150.0930.09521130.0820.20623160.4270.10821150.0040.0092318-0.144-0.10821150.0040.00923200.269-0.14721160.3220.01623190.1700.0672117-0.211-0.06923200.269-0.19221190.0020.1212322-0.0730.12221190.0020.1212323-0.181-0.0372120-0.0360.0952323-0.181-0.03721100.2260.0122400.1750.0002200.125-0.286243-0.037-0.0252220.125-0.286243-0.037-0.0172230.016-0.122<	21	5	0.127	-0.150	23	8	-0.033	0.018
2170.028 -0.037 23 100.048 -0.168 21 8 -0.308 0.038 23 110.1250.175 21 9 -0.044 0.080 23 12 -0.147 -0.242 21 10 -0.104 0.157 23 13 -0.086 0.098 21 110.183 -0.022 23 140.019 -0.244 21 120.098 -0.022 23 150.0930.099 21 130.0820.206 23 160.4270.108 21 14 -0.272 -0.024 23 17 -0.186 0.191 21 160.3220.016 23 190.1700.066 21 160.3220.01623200.269 -0.196 21 17 -0.211 -0.069 23200.269 -0.196 21 180.0410.0292321 -0.086 0.142 21 190.0020.1212322 -0.073 0.125 21 190.0020.1212323 -0.181 -0.086 21 190.0020.1212323 -0.181 -0.073 21 190.0020.12123240 0.175 0.000 22 00.1830.000241 -0.037 -0.038 22 1 -0.091 <td< td=""><td>21</td><td>6</td><td>0.075</td><td>-0.061</td><td>23</td><td>9</td><td>0.097</td><td>0.130</td></td<>	21	6	0.075	-0.061	23	9	0.097	0.130
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	21	7	0.028	-0.037	23	10	0.048	-0.168
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	8	-0.308	0.038	23	11	0.125	0.175
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	9	-0.044	0.080	23	12	-0.147	-0.242
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	10	-0.104	0.157	23	13	-0.086	0.098
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	11	0.183	-0.208	23	14	0.196	-0.249
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	12	0.098	-0.022	23	15	0.093	0.099
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	13	0.082	0.206	23	16	0.427	0.108
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	14	-0.272	-0.024	23	17	-0.186	0.191
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	15	0.004	0.009	23	18	-0.144	-0.108
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	16	0.322	0.016	23	19	0.170	0.067
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	17	-0.211	-0.069	23	20	0.269	-0.196
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	18	0.041	0.029	23	21	-0.086	0.142
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	19	0.002	0.121	23	22	-0.073	0.125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	20	-0.036	0.095	23	23	-0.181	-0.105
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	21	0.226	0.012	24	0	0.175	0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22	0	0.183	0.000	24	1	-0.037	-0.229
22 2 0.125 -0.286 24 3 -0.003 -0.077 22 3 0.016 -0.122 24 4 0.020 -0.033 22 4 0.011 -0.203 24 5 -0.171 0.258 22 5 0.010 -0.122 24 6 0.037 -0.011 22 6 -0.107 -0.230 24 7 -0.037 0.102 22 6 -0.107 -0.230 24 7 -0.037 0.102 22 7 -0.022 -0.005 24 8 0.254 -0.002 22 8 -0.317 0.136 24 9 -0.063 0.144 22 9 -0.006 0.129 24 10 0.207 -0.116 22 10 0.048 -0.076 24 11 -0.147 0.186 22 11 0.223 -0.068 24 12 -0.062 -0.093 22 12 -0.048 -0.081 24 13 -0.417 -0.014	22	1	-0.091	0.220	24	2	0.011	-0.073
22 3 0.016 -0.122 24 4 0.020 -0.033 22 4 0.011 -0.203 24 5 -0.171 0.258 22 5 0.010 -0.122 24 6 0.037 -0.011 22 6 -0.107 -0.230 24 7 -0.037 0.102 22 7 -0.022 -0.005 24 8 0.254 -0.002 22 8 -0.317 0.136 24 9 -0.063 0.144 22 9 -0.006 0.129 24 10 0.207 -0.116 22 10 0.048 -0.076 24 11 -0.147 0.186 22 11 0.223 -0.068 24 12 -0.062 -0.093 22 12 -0.048 -0.081 24 13 -0.417 -0.014	22	2	0.125	-0.286	24	3	-0.003	-0.077
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	3	0.016	-0.122	24	4	0.020	-0.033
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	4	0.011	-0.203	24	5	-0.171	0.258
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	5	0.010	-0.122	24	6	0.037	-0.011
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	6	-0.107	-0.230	24	7	-0.037	0.102
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	7	-0.022	-0.005	24	8	0.254	-0.002
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	8	-0.317	0.136	24	9	-0.063	0.144
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	9	-0.006	0 129	24	10	0.207	_0.116
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22	10	0.048	-0.076	24	11	-0.147	0 186
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22	11	0.223	-0.068	24	12	-0.062	_0.093
	22	12	-0.048	_0.081	24	13	-0.417	-0.014
22 13 0.05/ 0.344 24 14 0.151 -0.073	22	13	0.037	0.344	24	14	0.151	-0.073
22 14 -0.129 -0.187 24 15 -0.027 0.108 0.072	22	14	-0.129	-0.187	24	15	-0.027	0.108

Table 4 continued

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Table 4	continued			Table 4	continued		
n	т	Anm	Bnm	n	т	Anm	Bnm
24	16	0.040	-0.061	26	13	0.190	0.012
24	17	-0.143	0.014	26	14	0.269	0.057
24	18	-0.136	0.058	26	15	0.123	-0.028
24	19	0.102	0.002	26	16	-0.002	0.209
24	20	0.105	0.104	26	17	0.027	-0.471
24	21	-0.461	-0.186	26	18	-0.061	0.169
24	22	0.127	0.224	26	19	0.171	-0.123
24	23	-0.037	0.184	26	20	-0.250	-0.213
24	24	-0.209	0.015	26	21	-0.066	0.021
25	0	-0.019	0.000	26	22	0.097	0.133
25	1	-0.038	-0.014	26	23	0.148	0.117
25	2	-0.054	0.058	26	24	-0.118	-0.171
25	3	-0.035	-0.082	26	25	0.132	-0.225
25	4	-0.068	0.082	26	26	0.161	0.063
25	5	-0.101	0.084	27	0	-0.002	0.000
25	6	0.226	0.055	27	1	-0.007	-0.020
25	7	0.047	0.023	27	2	-0.102	0.036
25	8	0.278	0.073	27	3	-0.115	-0.028
25	9	-0.149	0.125	27	4	0.014	0.073
25	10	-0.044	0.037	27	5	0.132	0.016
25	10	-0.147	-0.034	27	6	0.029	0.010
25	12	-0.144	0.334	27	7	0.130	_0.220
25	12	-0.050	-0.064	27	8	-0.009	-0.220
25	14	0.142	-0.004	27	9	-0.009	-0.212
25	14	0.142	0.101	27	10	-0.048	-0.227
25	15	0.023	0.025	27	10	-0.134	-0.077
25	10	-0.075	0.149	27	12	-0.105	0.134
25	17	-0.017	-0.373	27	12	0.033	-0.075
25	10	-0.039	0.144	27	13	0.043	0.033
25	19	0.399	-0.038	27	14	0.102	-0.027
25	20	-0.237	0.021	27	15	-0.018	-0.080
25	21	0.088	0.031	27	10	0.040	-0.030
25	22	-0.189	0.210	27	17	0.217	-0.231
25	23	0.212	0.138	27	18	-0.020	0.108
25	24	0.091	-0.063	27	19	0.084	0.263
25	23	0.078	0.117	27	20	-0.331	-0.088
26	0	0.200	0.000	27	21	-0.294	-0.137
26	1	-0.039	0.056	27	22	0.169	0.173
26	2	-0.193	0.158	27	23	-0.171	0.165
26	3	-0.076	-0.045	27	24	-0.050	-0.334
26	4	-0.049	0.032	27	25	-0.199	0.083
26	5	0.105	-0.119	27	26	-0.082	-0.139
26	6	0.140	0.052	27	27	-0.165	-0.009
26	7	0.193	-0.148	28	0	0.142	0.000
26	8	0.103	-0.056	28	1	0.060	0.059
26	9	-0.080	-0.126	28	2	0.014	0.006
26	10	-0.257	0.032	28	3	0.150	-0.034
26	11	-0.163	0.008	28	4	0.089	0.037
26	12	-0.028	0.156	28	5	0.070	0.008

Table 4 continued

Table 4	continued			Table 4	continued		
n	т	Anm	Bnm	n	т	Anm	Bnm
28	6	0.021	0.068	29	25	-0.022	-0.079
28	7	0.032	-0.077	29	26	-0.228	0.039
28	8	-0.126	-0.100	29	27	0.365	-0.194
28	9	-0.091	-0.106	29	28	-0.051	-0.051
28	10	-0.001	0.099	29	29	0.158	0.039
28	11	0.032	0.038	30	0	0.196	0.000
28	12	0.166	0.156	30	1	0.148	0.094
28	13	0.069	-0.141	30	2	0.114	-0.015
28	14	-0.013	0.104	30	3	-0.075	0.094
28	15	-0.155	-0.136	30	4	0.003	-0.175
28	16	0.007	-0.025	30	5	-0.021	-0.108
28	17	0.201	0.030	30	6	-0.181	-0.140
28	18	-0.058	0.143	30	7	-0.093	-0.077
28	19	0.116	0.281	30	8	0.025	0.049
28	20	-0.119	-0.152	30	9	0.218	-0.080
28	21	-0.234	0.010	30	10	0.083	0.062
28	22	0.059	0.047	30	11	0.224	0.095
28	23	-0.052	-0.121	30	12	-0.061	-0.081
28	24	-0.126	-0.148	30	13	-0.057	-0.090
28	25	-0.220	-0.238	30	14	-0.171	-0.113
28	26	0.088	0.155	30	15	0.016	-0.026
28	27	-0.114	-0.039	30	16	-0.040	-0.140
28	28	0.144	0.047	30	17	0.215	0.060
29	0	0.059	0.000	30	18	-0.081	0.156
29	1	0.233	0.192	30	19	-0.013	0.043
29	2	-0.013	0.034	30	20	0.087	-0.234
29	3	0.199	0.020	30	21	-0.019	0.238
29	4	0.094	-0.085	30	22	0.069	-0.022
29	5	0.054	-0.149	30	23	-0.171	-0.268
29	6	-0.070	0.025	30	24	0.173	-0.057
29	7	0.023	-0.090	30	25	0.079	0.104
29	8	-0.093	0.053	30	26	0.001	0.045
29	9	-0.010	-0.037	30	27	-0.038	-0.197
29	10	0.149	0.288	30	28	0.036	-0.136
29	11	0.161	0.053	30	29	0.023	0.008
29	12	0.014	0.143	30	30	-0.128	-0.057
29	13	0.048	-0.201	31	0	0.009	0.000
29	14	-0.097	0.008	31	1	-0.109	-0.184
29	15	-0.151	-0.241	31	2	0.129	-0.010
29	16	0.050	-0.078	31	3	-0.004	0.082
29	17	0.020	0.071	31	4	0.046	-0.150
29	18	-0.077	0.162	31	5	-0.136	0.096
29	19	0.032	0.025	31	6	-0.075	_0 173
29	20	0.145	_0.025	31	7	-0.035	0.062
29	20	-0.085	0.200	31	, R	0.100	_0.002
29	21	0.181	_0.030	31	9	0.165	-0.090
29	22	_0.030	_0 133	31	10	_0.031	_0.055
29	23	0.059	_0.135	31	10	0.105	-0.003

Table 4 continued

Table 4	continued			Table 4	continued		
n	т	Anm	Bnm	n	т	Anm	Bnm
31	12	-0.010	-0.048	32	28	0.230	-0.134
31	13	0.130	0.034	32	29	0.109	0.132
31	14	-0.193	-0.034	32	30	0.131	0.142
31	15	0.201	0.262	32	31	-0.024	0.041
31	16	-0.136	-0.011	32	32	0.073	0.128
31	17	0.030	0.010	33	0	0.064	0.000
31	18	-0.186	0.060	33	1	-0.026	0.042
31	19	0.176	-0.065	33	2	0.031	0.043
31	20	0.058	-0.152	33	3	-0.135	-0.005
31	21	-0.122	0.204	33	4	-0.103	0.177
31	22	0.074	0.166	33	5	0.073	-0.104
31	23	-0.157	-0.170	33	6	-0.026	0.069
31	24	0.027	-0.074	33	7	-0.100	0.159
31	25	0.112	0.217	33	8	0.157	-0.063
31	26	-0.073	-0.264	33	9	-0.016	0.015
31	27	0.123	-0.130	33	10	0.057	-0.231
31	28	0.120	0.074	33	11	-0.214	0.034
31	29	-0.205	-0.070	33	12	0.052	0.019
31	30	0.081	-0.097	33	13	-0.101	0.189
31	31	-0.012	0.026	33	14	0.175	0.036
32	0	0.228	0.000	33	15	0.080	-0.004
32	1	-0.018	-0.175	33	16	0.002	-0.015
32	2	0.005	0.054	33	17	-0.060	-0.027
32	3	-0.004	0.055	33	18	-0.023	-0.177
32	4	-0.022	-0.042	33	19	0.066	0.054
32	5	-0.003	0.006	33	20	0.053	-0.004
32	6	0.088	-0.116	33	21	-0.219	0.125
32	7	0.077	0.136	33	21	0.124	0.008
32	8	0.194	-0.203	33	22	0.036	-0.173
32	9	-0.003	0.185	33	23	-0.048	-0.084
32	10	-0.013	-0.101	33	25	0.332	0.004
32	11	-0.064	_0.010	33	25	-0.103	0.028
32	12	-0.181	0.006	33	20	0.154	-0.103
32	12	0.137	0.190	33	28	-0.026	0.172
32	14	0.033	0.025	33	20	0.023	0.057
32	15	0.173	0.163	33	30	0.220	-0.270
32	16	0.027	_0.010	33	31	0.136	0.189
32	17	-0.044	-0.010	33	32	-0.171	0.185
32	18	-0.112	-0.262	33	32	-0.110	_0.012
32	10	0.038	-0.202	34	0	-0.110	-0.012
32	20	0.036	0.090	34	1	0.216	0.000
32	20	0.050	-0.103	24	1	-0.210	-0.000
32	21	-0.105	0.177	24	2	-0.077	-0.040
32 22	22	0.005	0.132	24	5	-0.042	-0.094
32 22	25	0.024	-0.354	54 24	4	0.108	0.266
32 22	24	-0.037	-0.014	54 24	5	-0.005	0.062
32 22	25	0.077	0.218	34 24	6	0.041	0.173
32 22	26	-0.076	-0.078	34 24	1	-0.033	-0.022
32	27	-0.024	-0.263	34	8	0.039	0.005

Table 4 continued

n Ann Bann n Ann Bunn 34 9 0.046 -0.034 35 22 0.109 0.063 34 10 0.020 -0.126 35 23 0.253 -0.233 34 11 -0.212 0.006 35 24 -0.272 0.188 34 12 0.233 0.017 35 25 0.056 -0.063 34 14 0.104 0.008 35 27 0.026 0.044 34 15 0.003 -0.084 35 28 0.087 -0.035 34 17 -0.108 -0.094 35 30 0.028 -0.017 34 19 0.032 -0.072 35 32 -0.448 0.036 34 21 -0.240 0.077 35 34 0.019 -0.071 34 22 0.271 0.075 36 1 0.231 <t< th=""><th>Table 4</th><th>continued</th><th></th><th></th><th>Table 4</th><th>continued</th><th></th><th></th></t<>	Table 4	continued			Table 4	continued		
44 9 0.046 -0.034 35 22 0.109 0.109 34 10 0.020 -0.126 35 23 0.233 -0.034 34 12 0.233 0.047 35 25 0.056 -0.068 34 13 -0.124 0.079 35 26 0.021 -0.133 34 15 0.003 -0.084 35 28 0.087 -0.035 34 16 0.057 -0.094 35 30 0.028 -0.017 34 19 0.032 -0.072 35 31 0.175 0.088 34 20 0.020 0.277 25 33 0.019 -0.133 34 21 -0.240 0.077 35 35 -0.043 0.073 34 22 0.274 0.065 35 35 -0.043 0.073 34 <th>n</th> <th>т</th> <th>Anm</th> <th>Bnm</th> <th>n</th> <th>т</th> <th>Anm</th> <th>Bnm</th>	n	т	Anm	Bnm	n	т	Anm	Bnm
34 10 0.020 -0.126 35 23 0.253 -0.283 34 11 -0.212 -0.06 25 24 -0.272 0.188 34 13 -0.124 0.079 35 26 0.021 -0.133 34 14 0.106 0.088 35 27 0.026 0.041 34 16 0.057 -0.109 25 29 -0.058 -0.133 34 17 -0.108 -0.072 35 31 0.175 0.0628 34 20 0.020 0.077 35 33 0.019 -0.138 34 21 -0.240 0.075 35 34 0.195 -0.075 34 22 0.074 0.075 36 1 0.233 0.063 0.088 34 23 0.071 50 1 0.233 0.063 0.043 0.063 34 24 -0.075	34	9	0.046	-0.034	35	22	0.109	0.109
3411 -0.212 -0.006 3524 -0.272 0.088 3412 0.233 0.047 3525 0.061 -0.016 3414 0.106 0.008 3527 0.026 0.041 3415 0.003 -0.084 3528 0.087 -0.033 3416 0.057 -0.109 3529 -0.455 -0.138 3417 -0.108 -0.094 3530 0.022 -0.071 3418 0.030 0.101 3531 0.175 0.083 3420 0.020 0.277 3534 0.019 -0.138 3421 -0.240 0.077 3534 0.019 -0.071 3423 0.099 -0.233 360 0.188 0.0071 3424 -0.207 0.075 361 0.231 0.063 3425 0.112 -0.144 362 -0.028 -0.044 3428 0.019 -0.224 365 0.192 -0.212 3430 0.018 0.015 367 0.022 -0.212 3430 0.018 0.015 367 0.022 -0.212 3433 0.0103 0.018 3611 0.043 0.068 3426 0.071 -0.225 3614 0.013 0.017 353 <t< td=""><td>34</td><td>10</td><td>0.020</td><td>-0.126</td><td>35</td><td>23</td><td>0.253</td><td>-0.283</td></t<>	34	10	0.020	-0.126	35	23	0.253	-0.283
3412 0.233 0.047 2525 0.056 -0.065 3413 -0.124 0.079 3526 0.021 -0.136 3414 0.005 -0.084 3528 0.087 -0.033 3416 0.057 -0.109 3530 0.028 -0.017 3418 0.030 -0.014 3531 0.175 0.067 3419 0.022 -0.077 3533 0.019 -0.138 3420 0.020 0.277 3533 0.019 -0.138 3421 -0.240 0.077 3534 0.195 -0.077 3423 0.099 -0.233 360 0.188 0.000 3424 -0.207 0.075 34 0.023 -0.044 3426 -0.075 -0.321 363 0.033 0.084 3427 0.055 0.656 4 0.013 0.084 3428 0.019 -0.024 365 0.192 0.044 3429 0.013 0.089 366 0.011 0.017 3430 0.018 0.015 56 110 0.043 0.059 3434 -0.088 -0.089 36 11 0.114 -0.022 3431 -0.038 0.060 36 13 0.040 0.015 35 1 -0.088	34	11	-0.212	-0.006	35	24	-0.272	0.188
3413 -0.124 0.079 3526 0.021 -0.133 3414 0.106 0.008 3527 0.026 0.041 3415 0.003 -0.084 3529 -0.055 -0.138 3416 0.057 -0.109 3529 -0.055 -0.138 3417 -0.108 -0.094 3531 0.175 0.087 3419 0.032 -0.072 3532 -0.448 0.066 3420 0.020 0.277 3534 0.019 -0.037 3422 0.274 0.077 3534 0.019 -0.077 3423 0.099 -0.233 360 0.188 0.006 3426 -0.175 -0.65 350 0.188 0.063 3428 0.019 -0.028 364 0.013 0.084 3429 0.013 0.089 366 0.041 0.011 3430 0.018 0.060 3611 0.022 -0.27 3431 -0.038 0.060 3613 0.060 0.011 3432 0.071 -0.025 369 0.069 0.012 3433 0.013 0.089 3610 0.043 0.055 3434 -0.038 -0.068 3611 0.134 0.022 353 $0.$	34	12	0.233	0.047	35	25	0.056	-0.065
34140.1060.00835270.0260.04134150.003-0.08435280.0657-0.13334160.037-0.108-0.04435300.028-0.0133417-0.108-0.04435300.028-0.01334190.032-0.07235330.019-0.13834200.0200.27735330.019-0.1383421-0.2400.07735340.0130.06134220.2740.0653535-0.0430.07734230.099-0.2333600.1880.00234250.112-0.104362-0.028-0.0143426-0.075-0.3213630.0330.08434270.0350.0583640.0130.04834280.019-0.0243650.1020.04434300.0180.0153670.022-0.2233431-0.0380.060368-0.0680.01134300.0180.0153670.022-0.2243431-0.0380.06036130.0400.0193530.0740.01836110.134-0.0253530.074	34	13	-0.124	0.079	35	26	0.021	-0.136
3415 0.003 -0.084 3528 0.087 -0.033 3416 0.057 -0.100 3529 -0.053 -0.138 3417 -0.108 -0.070 3530 0.028 -0.073 3419 0.022 -0.77 3532 -0.048 0.036 3420 0.020 0.777 3533 0.019 -0.138 3421 -0.240 0.077 3534 0.045 -0.075 3422 0.207 0.075 361 0.231 0.066 3423 0.099 -0.233 3600.188 0.006 3425 0.112 -0.104 362 -0.028 -0.014 3426 -0.075 -0.321 363 0.053 0.084 3427 0.350 0.058 364 0.013 0.084 3429 0.013 0.089 366 0.041 0.017 3430 0.018 0.065 3 0.069 -0.424 3430 0.018 0.066 3610 0.043 0.069 3433 0.010 0.68 3610 0.043 0.069 3433 0.051 -0.024 36 11 0.144 0.099 351 -0.026 0.076 3618 0.0107 0.122 353 0.051	34	14	0.106	0.008	35	27	0.026	0.041
3416 0.057 -0.109 3529 -0.055 -0.138 3417 -0.108 -0.094 3530 0.028 -0.017 3418 0.030 0.011 3531 0.175 0.087 3420 0.020 0.277 3533 0.019 -0.18 3421 -0.240 0.077 3534 0.195 -0.071 3422 0.274 0.065 3535 -0.043 0.071 3423 0.099 -0.233 36 0 0.188 0.006 3424 -0.207 0.075 -0.321 36 1 0.231 0.063 3425 0.112 -0.104 362 -0.028 -0.014 3426 -0.075 -0.321 363 0.053 0.064 3429 0.013 0.089 366 0.0141 0.017 3430 0.018 0.060 368 -0.068 0.011 3432 0.071 -0.025 369 0.069 -0.422 3433 0.013 0.018 0.660 3611 0.134 -0.022 353 0.051 -0.080 3611 0.134 -0.022 353 0.051 -0.080 3614 0.077 -0.164 369 0.168 3616 0.077 -0.128 36<	34	15	0.003	-0.084	35	28	0.087	-0.033
3417 -0.108 -0.094 3530 0.028 -0.017 34180.0300.01135310.1750.08334200.0200.27735330.019 -0.138 3421 -0.240 0.07735340.195 -0.071 34220.2740.0653535 -0.043 0.07134230.099 -0.233 3600.1880.00034250.112 -0.104 362 -0.028 -0.043 34250.019 -0.021 3630.0530.0843426 -0.075 -0.21 3630.0530.08434280.019 -0.024 3650.1920.04434290.0130.0893660.0410.0173431 -0.038 0.06638 -0.068 0.01134320.071 -0.25 3690.069 -0.422 34330.1030.11836100.0430.059351 -0.066 0.06636130.0400.0193520.071 -0.022 36110.134 -0.024 3530.0513617 -0.061 -0.214 3614 0.153 -0.017 3530.0510.0683613 0.040 <	34	16	0.057	-0.109	35	29	-0.055	-0.138
34180.0300.10135310.1750.08734190.032-0.0723532-0.4480.03334200.0200.27735330.019-0.1383421-0.2400.07735340.195-0.07734220.2740.0653535-0.0430.07134230.099-0.2333600.1880.0003424-0.2070.0753610.2310.06234250.112-0.14362-0.028-0.01434260.007-0.3213630.0530.08834270.3500.0583640.0130.04834290.0130.0983660.0410.01734300.0180.0153670.022-0.2123431-0.0380.006368-0.0680.01334320.017-0.0253690.069-0.4223500.2480.00036110.134-0.029351-0.0680.06636130.0400.0193520.0460.08536160.1070.1283610.0700.06836130.0400.0193530.055-0.030362	34	17	-0.108	-0.094	35	30	0.028	-0.017
3419 0.032 -0.072 35 32 -0.448 0.036 3420 0.020 0.277 35 33 0.019 -0.18 3421 -0.240 0.077 35 34 0.195 -0.073 3422 0.274 0.065 35 35 -0.043 0.071 3423 0.099 -0.233 36 0 0.188 0.060 3424 -0.207 0.075 36 1 0.231 0.063 3425 0.112 -0.14 36 2 -0.028 -0.014 3426 -0.075 -0.321 36 3 0.053 0.084 3429 0.013 0.089 36 6 0.041 0.017 3430 0.018 0.015 36 7 0.022 -0.22 3433 0.018 0.015 36 7 0.022 -0.22 3433 0.018 0.018 36 11 0.134 0.099 34 33 0.013 0.084 30.099 0.66 0.011 34 34 -0.086 -0.089 36 14 0.153 0.017 35 3 0.051 -0.024 36 15 0.072 -0.16 35 3 0.051 -0.026 36 13 0.044 0.099 35 3 0.051 -0.026 36 13 <td< td=""><td>34</td><td>18</td><td>0.030</td><td>0.101</td><td>35</td><td>31</td><td>0.175</td><td>0.087</td></td<>	34	18	0.030	0.101	35	31	0.175	0.087
34200.0200.27735330.019 -0.138 3421 -0.240 0.07735340.195 -0.071 34220.2740.0653535 -0.043 0.07134230.099 -0.233 3600.1880.0023424 -0.207 0.0753610.2310.06234250.112 -0.104 362 -0.028 -0.014 3426 -0.075 -0.321 3630.0530.04834270.3500.0583640.0130.04834290.0130.0893650.1920.04434300.0180.0153670.022 -0.212 3431 -0.038 0.060368 -0.068 0.01134320.071 -0.025 3690.069 -0.420 34330.0130.11836100.0430.0553434 -0.088 -0.089 36110.134 -0.022 351 -0.046 0.00636130.0170.1223530.051 -0.024 36150.072 -0.161 3530.051 -0.024 36140.153 -0.017 3670.0250.07636180.0130.01535<	34	19	0.032	-0.072	35	32	-0.448	0.036
3421 -0.240 0.077 3534 0.195 -0.077 3422 0.274 0.065 3535 -0.043 0.071 3423 0.099 -0.233 360 0.188 0.000 3424 -0.207 0.075 361 0.231 0.062 3425 0.112 -0.104 362 -0.028 -0.014 3426 -0.075 -0.321 363 0.053 0.084 3429 0.013 0.089 366 0.041 0.014 3430 0.018 0.015 367 0.022 -0.212 3431 -0.038 0.060 368 -0.068 0.011 3432 0.071 -0.025 369 0.066 -0.422 3433 0.03 0.118 3610 0.043 0.059 3434 -0.088 -0.089 3611 0.134 -0.025 351 -0.024 3613 0.017 0.025 353 0.051 -0.024 3615 0.072 -0.166 351 -0.026 3616 0.107 0.125 353 0.051 -0.024 3615 0.072 -0.166 353 0.051 -0.024 3616 0.107 0.125 351 -0.016 0.066 36	34	20	0.020	0.277	35	33	0.019	-0.138
3422 0.274 0.065 35 35 -0.043 0.071 3423 0.099 -0.233 36 0 0.188 0.000 3424 -0.207 0.075 36 1 0.231 0.063 3425 0.112 -0.014 36 2 -0.028 -0.014 3426 -0.075 -0.321 36 3 0.053 0.084 3427 0.350 0.058 36 4 0.013 0.048 3429 0.013 0.089 36 6 0.041 0.017 3430 0.018 0.015 36 7 0.022 -0.212 3431 -0.038 0.060 36 8 -0.069 0.011 3432 0.071 -0.025 36 9 0.069 -0.424 3433 0.103 0.118 36 10 0.043 0.055 34 33 0.103 0.118 36 10 0.043 0.055 35 0 -0.024 36 11 0.134 -0.026 35 3 0.051 -0.026 36 13 0.040 0.019 35 3 0.051 -0.080 36 14 0.133 0.015 35 5 0.074 0.119 36 17 -0.091 -0.125 35 5 0.074 0.016 36 22 0.6	34	21	-0.240	0.077	35	34	0.195	-0.077
34 23 0.099 -0.233 36 0 0.188 0.000 34 24 -0.207 0.075 36 1 0.231 0.062 34 26 -0.075 -0.21 36 3 0.083 0.044 34 27 0.350 0.058 36 4 0.013 0.048 34 28 0.019 -0.024 36 5 0.192 0.044 34 29 0.018 0.053 36 8 -0.068 0.011 34 30 0.018 0.060 36 8 -0.068 0.011 34 32 0.071 -0.025 36 9 0.069 -0.420 34 31 -0.038 0.060 36 8 -0.068 0.011 34 32 0.071 -0.025 36 9 0.069 -0.420 34 31 -0.038 0.060 36 13 0.040 0.015 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.066 0.066 36 13 0.040 0.015 35 5 0.074 0.119 36 17 0.091 -0.128 35 5 0.074 0.165 36 16 0.107 0.128 35 7 0.098 -0.165 23 0.047 0.007 35 16 0.029 <	34	22	0.274	0.065	35	35	-0.043	0.071
34 24 -0.207 0.075 36 1 0.231 0.062 34 25 0.112 -0.104 36 2 -0.028 -0.014 34 26 -0.075 -0.321 36 3 0.053 0.088 34 27 0.350 0.058 36 4 0.013 0.088 34 29 0.013 0.089 36 6 0.041 0.017 34 30 0.018 0.015 36 7 0.022 -0.213 34 31 -0.038 0.060 36 8 -0.069 -0.426 34 32 0.071 -0.025 36 9 0.069 -0.426 34 31 -0.038 0.060 36 11 0.134 -0.022 34 34 -0.088 -0.089 36 11 0.134 -0.024 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.066 0.006 36 13 0.040 0.019 35 3 0.051 -0.024 36 17 -0.091 -0.128 35 5 0.074 0.119 36 17 -0.091 -0.128 35 5 0.072 -0.166 36 18 0.103 0.015 35 7 0.998 -0.165 36 18 0.103 0.015 35 10	34	23	0.099	-0.233	36	0	0.188	0.000
34 25 0.112 -0.104 36 2 -0.028 -0.014 34 26 -0.075 -0.321 36 3 0.053 0.084 34 27 0.350 0.058 36 4 0.013 0.084 34 29 0.013 0.089 36 6 0.041 0.017 34 30 0.018 0.015 36 7 0.022 -0.212 34 31 -0.038 0.060 36 8 -0.068 0.011 34 32 0.071 -0.25 36 9 0.069 -0.422 34 33 0.103 0.118 36 10 0.043 0.059 34 34 -0.088 -0.089 36 11 0.134 -0.025 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.066 0.006 36 13 0.040 0.019 35 3 0.051 -0.024 36 15 0.072 -0.166 35 4 0.160 0.85 36 16 0.107 0.123 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 22 0.063 0.143 35 10	34	24	-0.207	0.075	36	1	0.231	0.062
34 26 -0.075 -0.321 36 3 0.053 0.084 34 27 0.350 0.058 36 4 0.013 0.044 34 28 0.019 -0.024 36 5 0.192 0.044 34 30 0.018 0.015 36 7 0.022 -0.212 34 31 -0.038 0.060 36 8 -0.068 0.011 34 32 0.071 -0.025 36 9 0.069 -0.420 34 34 -0.088 -0.089 36 11 0.134 -0.025 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.006 0.006 36 13 0.040 0.019 35 2 -0.166 -0.024 36 15 0.072 -0.166 35 4 0.160 0.085 36 14 0.133 -0.016 35 5 0.074 0.119 36 17 -0.091 -0.125 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 22 0.063 0.143 35 10 0.070 0.688 36 22 0.663 0.143 35 11 <	34	25	0.112	-0.104	36	2	-0.028	-0.014
34 27 0.350 0.058 36 4 0.013 0.048 34 28 0.019 -0.024 36 5 0.192 0.044 34 29 0.013 0.089 36 6 0.041 0.017 34 30 0.018 0.015 36 7 0.022 -0.212 34 31 -0.038 0.060 36 8 -0.066 0.011 34 32 0.071 -0.25 36 9 0.069 -0.420 34 33 0.103 0.118 36 10 0.043 0.059 34 34 -0.088 -0.089 36 11 0.134 -0.020 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.066 0.006 36 13 0.040 0.019 35 3 0.051 -0.024 36 15 0.072 -0.161 35 5 0.074 0.119 36 17 -0.091 -0.125 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.24 35 8 -0.055 -0.030 36 20 -0.099 -0.161 35 10 0.070 0.68 36 22 0.63 0.445 35 10 <	34	26	-0.075	-0.321	36	3	0.053	0.084
34 28 0.019 -0.024 36 5 0.192 0.044 34 29 0.013 0.089 36 6 0.041 0.017 34 30 0.018 0.015 36 7 0.022 -0.212 34 31 -0.038 0.060 36 8 -0.068 0.011 34 32 0.071 -0.025 36 9 0.069 -0.420 34 33 0.103 0.118 36 10 0.043 0.059 34 34 -0.088 -0.089 36 11 0.134 -0.020 35 0 -0.248 0.000 36 12 -0.164 0.093 35 1 -0.026 0.066 36 13 0.040 0.019 35 2 -0.146 -0.080 36 14 0.153 -0.072 35 3 0.051 -0.024 36 15 0.072 -0.164 35 5 0.074 0.119 36 17 -0.091 -0.128 35 5 0.074 0.119 36 12 0.061 0.019 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 20 -0.099 -0.161 35 10 0.070 0.068 36 21 0.129 -0.158 35 1	34	27	0.350	0.058	36	4	0.013	0.048
34 29 0.013 0.089 36 6 0.041 0.017 34 30 0.018 0.015 36 7 0.022 -0.212 34 31 -0.038 0.060 36 8 -0.068 0.011 34 32 0.071 -0.025 36 9 0.069 -0.420 34 33 0.103 0.118 36 10 0.043 0.059 34 34 -0.088 -0.089 36 11 0.134 -0.020 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.006 0.066 36 13 0.040 0.017 35 3 0.051 -0.024 36 15 0.072 -0.107 35 3 0.051 -0.024 36 15 0.072 -0.107 35 5 0.074 0.119 36 17 -0.091 -0.125 35 5 0.074 0.119 36 17 -0.091 -0.124 35 8 -0.055 -0.030 36 22 0.063 0.145 35 10 0.070 0.668 36 22 0.063 0.145 35 10 0.070 0.668 36 22 0.063 0.145 35 10 0.071 0.068 36 22 0.063 0.145 35 10 </td <td>34</td> <td>28</td> <td>0.019</td> <td>-0.024</td> <td>36</td> <td>5</td> <td>0.192</td> <td>0.044</td>	34	28	0.019	-0.024	36	5	0.192	0.044
34 30 0.018 0.015 36 7 0.022 -0.212 34 31 -0.038 0.060 36 8 -0.068 0.011 34 32 0.071 -0.025 36 9 0.069 -0.420 34 33 0.103 0.118 36 10 0.043 0.059 34 -0.088 -0.089 36 11 0.134 -0.029 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.006 0.006 36 13 0.040 0.019 35 2 -0.146 -0.080 36 14 0.153 -0.017 35 3 0.051 -0.024 36 15 0.072 -0.106 35 4 0.160 0.085 36 16 0.107 0.125 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 20 -0.009 -0.016 35 7 0.098 -0.165 36 18 0.103 0.015 35 10 0.070 0.668 36 21 0.129 -0.159 35 10 0.070 0.668 36 22 0.663 0.441 35 14 $0.$	34	29	0.013	0.089	36	6	0.041	0.017
34 31 -0.038 0.060 36 8 -0.068 0.011 34 32 0.071 -0.025 36 9 0.069 -0.420 34 33 0.103 0.118 36 10 0.043 0.059 34 34 -0.088 -0.089 36 11 0.134 -0.020 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.006 0.006 36 13 0.040 0.019 35 2 -0.146 -0.080 36 14 0.153 -0.017 35 3 0.051 -0.024 36 15 0.072 -0.160 35 4 0.160 0.085 36 16 0.107 0.128 35 5 0.074 0.119 36 17 -0.091 -0.125 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 22 0.063 0.145 35 10 0.070 0.68 36 22 0.063 0.145 35 11 -0.038 -0.061 36 23 0.047 0.077 35 13 -0.029 -0.172 36 27 -0.149 0.074 35	34	30	0.018	0.015	36	7	0.022	-0.212
34 32 0.071 -0.025 36 9 0.069 -0.420 34 33 0.103 0.118 36 10 0.043 0.059 34 34 -0.088 -0.089 36 11 0.134 -0.020 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.006 0.006 36 13 0.040 0.019 35 2 -0.146 -0.080 36 14 0.153 -0.017 35 3 0.051 -0.024 36 15 0.072 -0.166 35 4 0.160 0.085 36 16 0.107 0.128 35 5 0.074 0.119 36 17 -0.091 -0.128 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 22 0.063 0.143 35 10 0.070 0.068 36 22 0.063 0.143 35 11 -0.038 -0.061 36 23 0.047 0.077 35 12 -0.015 0.187 36 27 -0.188 0.024 35 14 0.173 0.007 36 27 -0.149 0.074 35	34	31	-0.038	0.060	36	8	-0.068	0.011
34 33 0.103 0.118 36 10 0.043 0.053 34 34 -0.088 -0.089 36 11 0.134 -0.020 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.006 0.006 36 13 0.040 0.019 35 2 -0.146 -0.080 36 14 0.153 -0.017 35 3 0.051 -0.024 36 15 0.072 -0.106 35 4 0.160 0.085 36 16 0.107 0.128 35 5 0.074 0.119 36 17 -0.091 -0.123 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 20 -0.009 -0.166 35 10 0.070 0.068 36 22 0.063 0.145 35 11 -0.038 -0.061 36 23 0.047 0.076 35 12 -0.015 0.187 36 24 -0.198 0.180 35 14 0.173 0.007 36 26 0.090 -0.232 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 <	34	32	0.071	-0.025	36	9	0.069	-0.420
34 34 -0.088 -0.089 36 11 0.134 -0.024 35 0 -0.248 0.000 36 12 -0.164 0.099 35 1 -0.006 0.006 36 13 0.040 0.019 35 2 -0.146 -0.080 36 14 0.153 -0.017 35 3 0.051 -0.024 36 15 0.072 -0.166 35 4 0.160 0.085 36 16 0.107 0.128 35 5 0.074 0.119 36 17 -0.091 -0.125 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 20 -0.009 -0.161 35 9 0.129 -0.209 36 21 0.129 -0.159 35 10 0.070 0.068 36 22 0.063 0.145 35 11 -0.038 -0.061 36 23 0.047 0.007 35 12 -0.015 0.187 36 24 -0.198 0.180 35 14 0.173 0.007 36 26 0.090 -0.232 35 16 0.143 -0.091 36 27 -0.149 0.074 35 16 0.1	34	33	0.103	0.118	36	10	0.043	0.059
350 -0.248 0.000 36 12 -0.164 0.009 35 1 -0.006 0.006 36 130.0400.019 35 2 -0.146 -0.080 36 140.153 -0.017 35 30.051 -0.024 36 150.072 -0.166 35 40.1600.085 36 160.1070.128 35 50.0740.119 36 17 -0.091 -0.125 35 60.2650.076 36 180.1030.015 35 70.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.30 36 20 -0.009 -0.166 35 90.129 -0.209 36 21 0.129 -0.159 35 100.0700.068 36 220.0630.145 35 11 -0.038 -0.061 36 230.0470.007 35 12 -0.015 0.187 36 24 -0.198 0.180 35 140.1730.007 36 260.090 -0.232 35 160.143 -0.091 36 280.0470.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 <td>34</td> <td>34</td> <td>-0.088</td> <td>-0.089</td> <td>36</td> <td>11</td> <td>0.134</td> <td>-0.020</td>	34	34	-0.088	-0.089	36	11	0.134	-0.020
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35	0	-0.248	0.000	36	12	-0.164	0.099
35 2 -0.146 -0.080 36 14 0.153 -0.017 35 3 0.051 -0.024 36 15 0.072 -0.106 35 4 0.160 0.085 36 16 0.107 0.128 35 5 0.074 0.119 36 17 -0.091 -0.125 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 20 -0.009 -0.016 35 9 0.129 -0.209 36 21 0.129 -0.159 35 10 0.070 0.068 36 22 0.063 0.145 35 11 -0.038 -0.061 36 23 0.047 0.007 35 12 -0.015 0.187 36 24 -0.198 0.180 35 13 -0.021 0.121 36 25 0.128 0.029 35 14 0.173 0.007 36 26 0.090 -0.232 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 19 -0.134 -0.079 36 31 -0.034 0.033 35 <td>35</td> <td>1</td> <td>-0.006</td> <td>0.006</td> <td>36</td> <td>13</td> <td>0.040</td> <td>0.019</td>	35	1	-0.006	0.006	36	13	0.040	0.019
35 3 0.051 -0.024 36 15 0.072 -0.106 35 4 0.160 0.085 36 16 0.107 0.128 35 5 0.074 0.119 36 17 -0.091 -0.125 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 20 -0.009 -0.166 35 9 0.129 -0.209 36 21 0.129 -0.159 35 10 0.070 0.068 36 22 0.063 0.145 35 11 -0.038 -0.061 36 23 0.047 0.007 35 12 -0.015 0.187 36 24 -0.198 0.180 35 13 -0.021 0.121 36 25 0.128 0.023 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 19 -0.134 -0.079 36 31 -0.034 0.033 35 20 -0.043 0.204 36 33 -0.245 0.139 <td>35</td> <td>2</td> <td>-0.146</td> <td>-0.080</td> <td>36</td> <td>14</td> <td>0.153</td> <td>-0.017</td>	35	2	-0.146	-0.080	36	14	0.153	-0.017
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	35	3	0.051	-0.024	36	15	0.072	-0.106
35 5 0.074 0.119 36 17 -0.091 -0.125 35 6 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 20 -0.009 -0.016 35 9 0.129 -0.209 36 21 0.129 -0.159 35 10 0.070 0.068 36 22 0.063 0.145 35 11 -0.038 -0.061 36 23 0.047 0.007 35 12 -0.015 0.187 36 24 -0.198 0.180 35 13 -0.021 0.121 36 25 0.128 0.029 35 14 0.173 0.007 36 26 0.090 -0.232 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 <	35	4	0.160	0.085	36	16	0.107	0.128
356 0.265 0.076 36 18 0.103 0.015 35 7 0.098 -0.165 36 19 -0.161 -0.214 35 8 -0.055 -0.030 36 20 -0.009 -0.016 35 9 0.129 -0.209 36 21 0.129 -0.159 35 10 0.070 0.068 36 22 0.063 0.145 35 11 -0.038 -0.061 36 23 0.047 0.007 35 12 -0.015 0.187 36 24 -0.198 0.180 35 13 -0.021 0.121 36 25 0.128 0.029 35 14 0.173 0.007 36 26 0.090 -0.232 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	5	0.074	0.119	36	17	-0.091	-0.125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35	6	0.265	0.076	36	18	0.103	0.015
35 8 -0.055 -0.030 36 20 -0.009 -0.016 35 9 0.129 -0.209 36 21 0.129 -0.159 35 10 0.070 0.068 36 22 0.063 0.145 35 11 -0.038 -0.061 36 23 0.047 0.007 35 12 -0.015 0.187 36 24 -0.198 0.180 35 13 -0.021 0.121 36 25 0.128 0.029 35 14 0.173 0.007 36 26 0.090 -0.232 35 16 0.143 -0.091 36 28 0.047 0.207 35 16 0.143 -0.091 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	7	0.098	-0.165	36	19	-0.161	-0.214
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	35	8	-0.055	-0.030	36	20	-0.009	-0.016
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35	9	0.129	-0.209	36	21	0.129	-0.159
35 11 -0.038 -0.061 36 23 0.047 0.007 35 12 -0.015 0.187 36 24 -0.198 0.180 35 13 -0.021 0.121 36 25 0.128 0.029 35 14 0.173 0.007 36 26 0.090 -0.232 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	10	0.070	0.068	36	22	0.063	0.145
35 11 3000 300 20 0001 20 0001 0001 35 12 -0.015 0.187 36 24 -0.198 0.180 35 13 -0.021 0.121 36 25 0.128 0.029 35 14 0.173 0.007 36 26 0.090 -0.232 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	11	-0.038	-0.061	36	23	0.047	0.007
35 12 0.015 0.101 36 21 0.196 0.106 35 13 -0.021 0.121 36 25 0.128 0.029 35 14 0.173 0.007 36 26 0.090 -0.232 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	12	-0.015	0.187	36	23	-0.198	0.180
35 16 0.021 0.021 0.021 0.021 0.025 35 14 0.173 0.007 36 26 0.090 -0.232 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	13	-0.021	0.121	36	25	0.128	0.029
35 11 0.015 0.001 36 20 0.050 0.015 35 15 -0.029 -0.172 36 27 -0.149 0.074 35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	14	0.173	0.007	36	25	0.090	-0.232
35 16 0.143 -0.091 36 28 0.047 0.207 35 17 -0.102 -0.168 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	15	-0.029	_0 172	36	20	-0 149	0.074
35 17 -0.102 -0.168 36 20 0.047 0.107 35 18 0.019 0.101 36 29 -0.360 -0.341 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	16	0.143	_0.091	36	28	0.047	0.207
35 17 0.102 -0.100 36 29 -0.300 -0.041 35 18 0.019 0.101 36 30 0.064 0.014 35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	17	_0.102	_0.091 _0.168	36	20	_0.360	_0 3/1
35 19 -0.134 -0.079 36 31 -0.034 0.053 35 20 -0.043 0.204 36 32 0.003 0.139 35 21 0.055 -0.018 36 33 -0.245 0.132	35	18	0.019	0.100	36	30	0.064	-0.341
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35	10	_0 134	_0.079	36	31	_0.034	0.014
35 21 0.055 -0.018 36 33 -0.245 0.139	35	20	_0.043	0.079	36	32	0.003	0.000
	35	20	0.055	_0.018	36	32	_0.245	0.139

Table 4 continued

n	т	Anm	Bnm
36	34	-0.178	0.053
36	35	0.082	-0.189
36	36	0.000	0.039

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